A discussion on the paper "Estimates of CO₂ traffic emissions from mobile concentration measurements"

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Outline

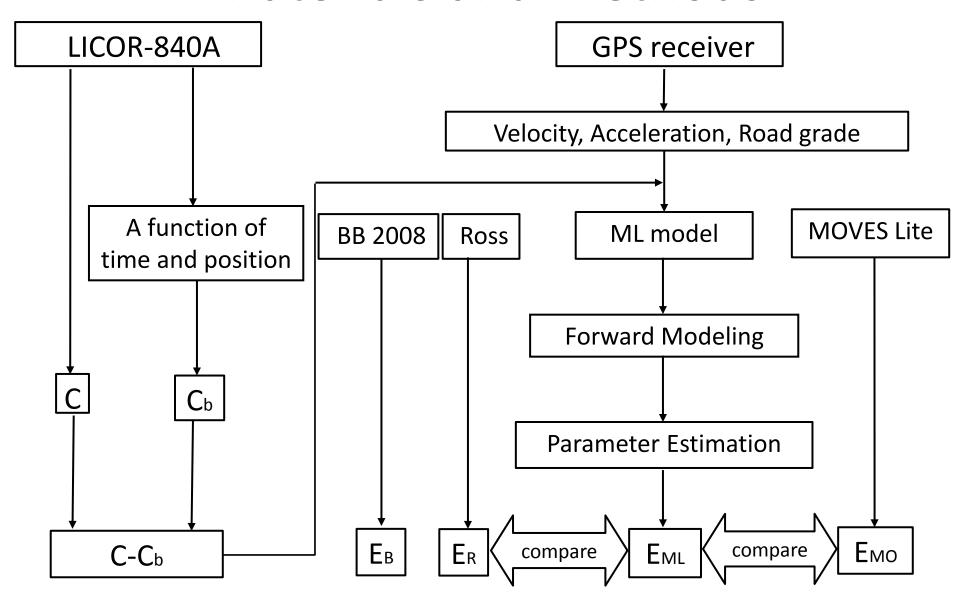
- Introduction
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Introduction

- Urban area plays a disproportionately large part (>70%) of fossil fuel CO₂ emission in the worldwide range [Duren and Miller, 2012]. Within the urban core, The dominant source of emissions often is the traffic [Erickson et al., 2013].
- There are several challenges:
 - 1. Concentration data requires a high spatial and temporal resolution.
 - 2. The influence of **traffic conditions** on the boundary conditions for CO₂ dilution and pollutant dispersal.
- The objective of this experiment is to derive on-road emissions and develop a model for on-road concentrations, we then use data to infer instantaneous emission rates.



Fig. 1 Map of trip route along California State Route 24.



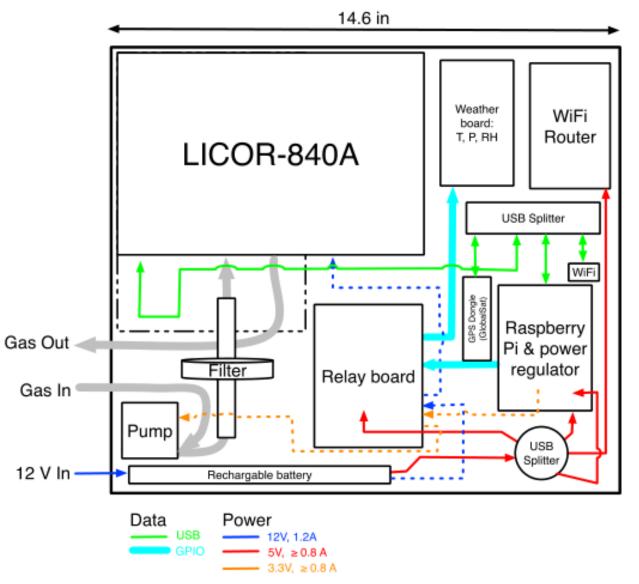


Fig. 2 Illustration of prototype node used in this experiment.

Materials and Methods Model for Roadway CO₂ Concentration

$$C-C_{\rm b}$$
 $\sim FEv^{-4/3}$ (Baker, 1996)

$$F = \frac{v}{d} N_{\text{lanes}} \qquad d^{-1} = \left(\frac{W_{\text{car}}/2}{\tan\left(\theta_{\text{car}}/2\right)} + l_{\text{car}} - l_{\text{cam}}\right)^{-1}$$

$$C - C_b = \kappa \frac{EN_{lanes}}{d} v^{-1/3}$$

Total highway emissions : $Q = \frac{E/V_{lanes}}{d}$

$$C - C_b = \kappa Q v^{-1/3}$$

Model for Roadway CO2 Concentration

$$Q = \frac{EN_{\text{lanes}}}{d}$$

The per car emission rate: $E = P_{\rm f} f_{\rm c} f_{\rm oxid} f_{\rm m}$

The vehicle fuel consumption rate:

$$P_{\rm f} = \frac{1}{\eta_{\rm t}} \left(\frac{f_0 V N}{2000} + P_{\rm acc} + \frac{1 - c}{\varepsilon} H \left\{ P_{\rm load} \right\} \right) \text{ (Ross, 1994, 1997)}$$

The engine speed :
$$N = \frac{f_{\rm N}}{1 + \left(v/v_{\rm t}\right)^{-6}} + N_{\rm idle}$$

(Thomas and Ross, 1997)

Model for Roadway CO2 Concentration

The engine load:
$$P_{\text{load}} = P_{\text{roll}} + P_{\text{air}} + P_{\text{inertia}} + P_{\text{grade}}$$
 (Ross, 1997)

$$P_{\text{roll}} = C_{\text{R}} Mgv$$
 $P_{\text{air}} = 0.5 \rho C_{\text{d}} A v^3 / 1000$

$$P_{\text{inertia}} = f_{\text{i}} M v a$$
 $P_{\text{grade}} = M g v \sin \theta$

$$C - C_{\rm b} = N_{\rm lanes} v^{-1/3} d^{-1} \left(k_{\rm fro,acc} + k_{\rm fro,N} \frac{1}{1 + (v/v_{\rm t})^{-6}} + H \left\{ k_{\rm roll} v + k_{\rm air} v^3 + k_{\rm inertia} v a + k_{\rm grade} v \sin(\tan^{-1}\theta) \right\} \right)$$

Table 1. Model Parameter Summary ^a				
Coefficient	Definition	Prior Bounds	Result	Result/Expected ^b
k _{fr0,acc}	$\kappa \frac{f_c f_{\text{oxid}} f_m}{\eta_t} \left(\frac{f_0 V N_{\text{idle}}}{2000} + P_{\text{acc}} \right)$	12-3200	98.0 ^{+10.4} -10.0	0.20
$k_{\rm fr0,N}$	$\kappa \frac{f_c f_{\text{oxid}} f_m}{\eta_t} \frac{f_0 V}{2000} f_N$	14-5400	757 ⁺¹⁹	1.2
$k_{\rm roll}$	$\kappa \frac{f_c f_{oxid} f_m}{\eta_t} \frac{1-c}{e} C_R M g$	2.0-200	$64.1^{+2.6}_{-3.4}$	3.0
k_{air}	$\kappa \frac{f_c f_{oxid} f_m}{\eta_t} \frac{1-c}{\epsilon} \frac{0.5 \rho C_D A}{1000}$	0.0050-0.30	$0.0586^{+0.0040}_{-0.0033}$	0.91
$k_{inertia}$	$\kappa \frac{f_c f_{\text{oxid}} f_m}{\eta_t} \frac{1-c}{\epsilon} f_i M$	30-1100	215 ⁺³ ₋₃	0.87
$k_{\rm grade}$	$\kappa \frac{f_c f_{\text{oxid}} f_m}{\eta_t} \frac{1-c}{\epsilon} M g$	280-10000	1800^{+13}_{-13}	0.77

^aResults correspond to 16%, 50%, and 84% in the marginalized distributions.

^bAssumes $\kappa = 0.00137$ (see text).

Materials and Methods Model for Roadway CO₂ Concentration

$$C - C_{\rm b} = \kappa N_{\rm lanes} v^{-1/3} d^{-1} \left(E_{\rm fro,acc} + E_{\rm fro,N} + E_{\rm roll} + E_{\rm air} + E_{\rm inertia} + E_{\rm grade} \right)$$

fro, acc: accessories and idling engine friction at zero load

fro, N: the increase with engine speed in engine friction at zero load

roll: rolling resistance

air: air drag

inertia: inertia

grade: road grade

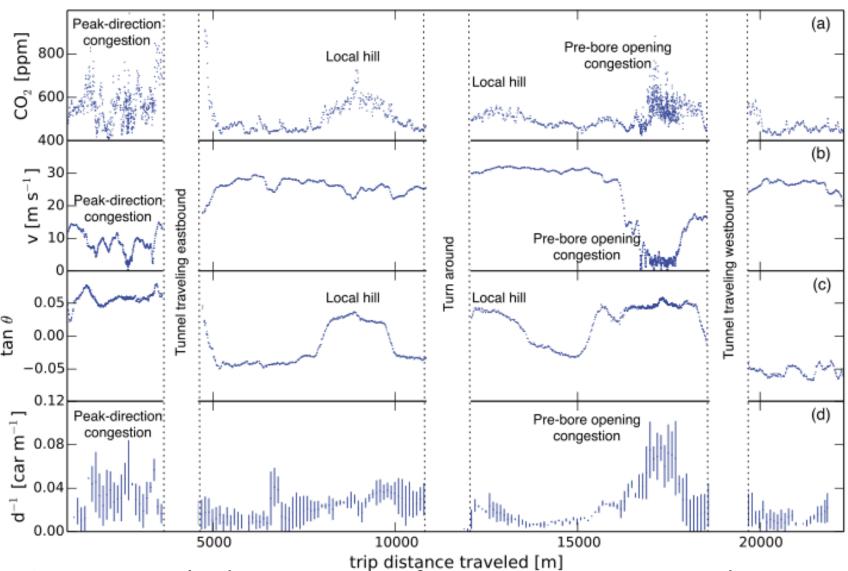


Fig. 3 Example data sequence for one evening trip made prior to the opening of the fourth bore.

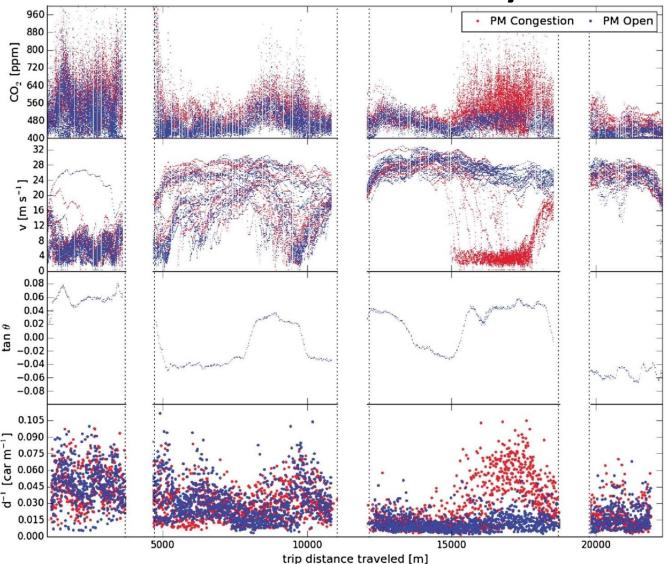


Fig. 4 Example data sequence for the full evening data set made prior to the opening of the fourth bore.

Forward Modeling

Q, the total highway surface emission rate, is relatively insensitive to congestion, because Q is approximately independent of vehicle speed.

The velocity correction for vehicle-induced turbulence does a reasonable job of predicting concentrations.

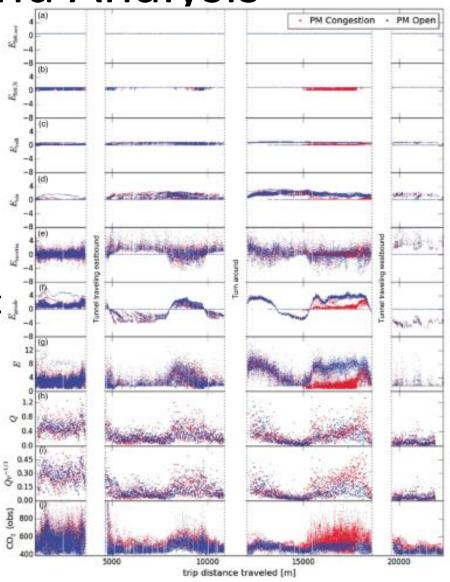


Fig.5 Forward modeling results for all evening data.

Results and Analysis Parameter Estimation

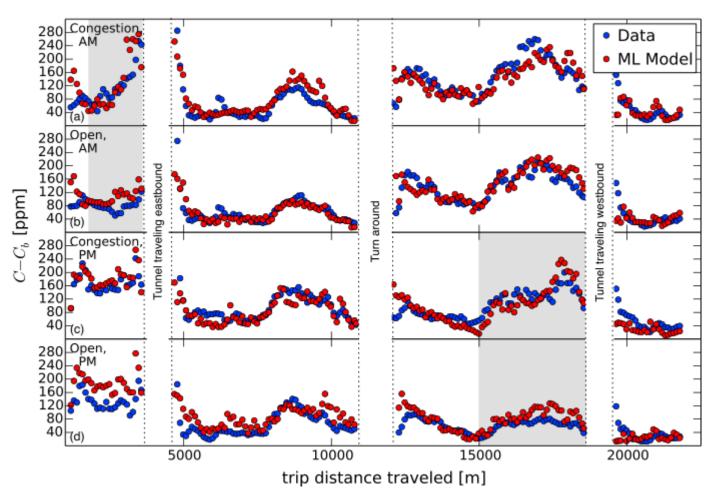


Fig. 6 Comparison of the Highway 24 concentration data above background to the maximum likelihood model.

Results and Analysis Parameter Estimation

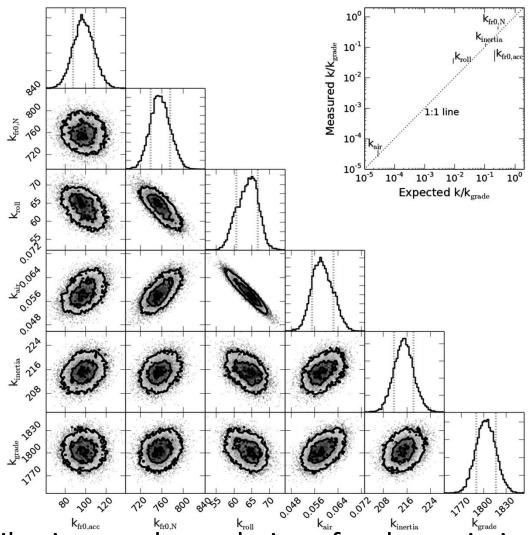


Fig. 7 The distributions and correlations for the emissions rate constants.

Three emissions models

- Ross model: velocity, acceleration, and road grade [Ross, 1994, 1997]
- BB08: its only input is speed [Barth and Boriboonsomsin, 2008]
- MOVES Lite: velocity, acceleration, and road grade [Frey and Liu, 2013]

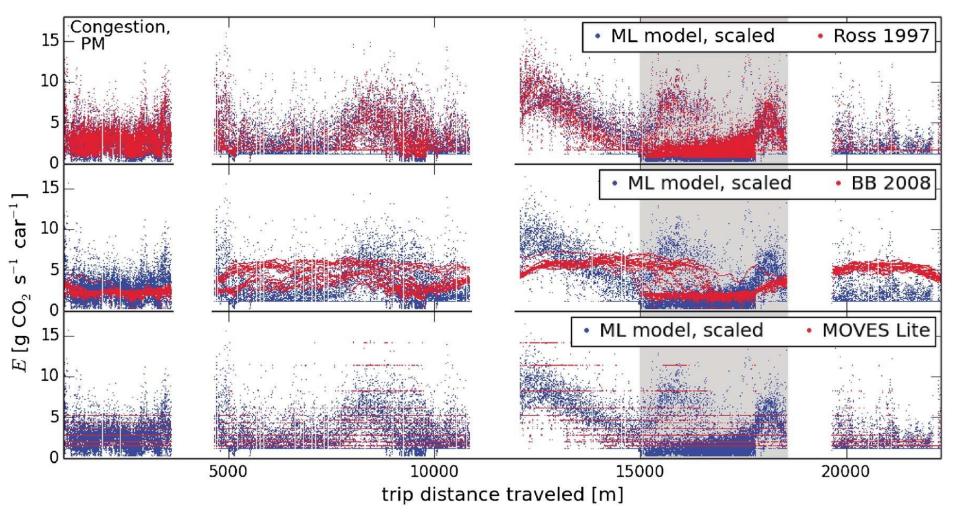


Fig. 8 Instantaneous vehicle emission rates for our maximum likelihood model compared to three alternative models presented in the literature.

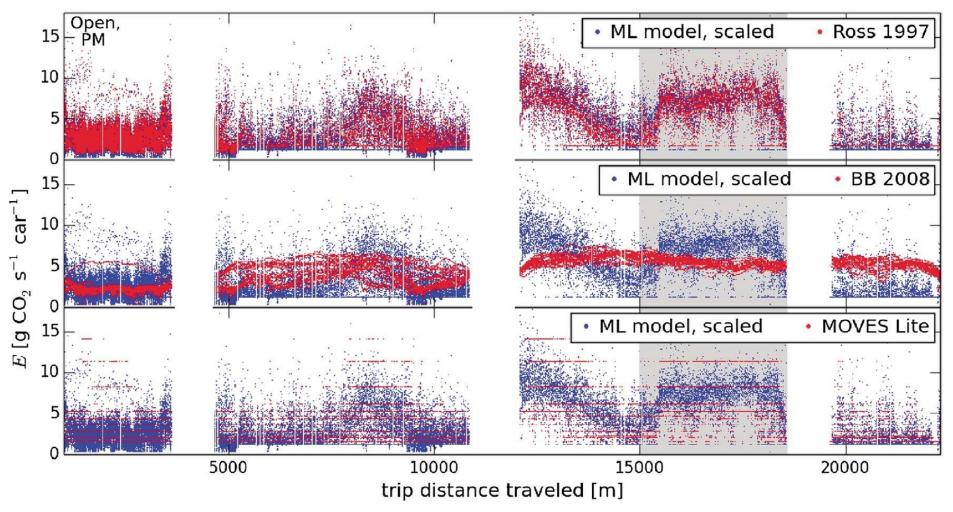


Fig. 9 Same as Figure 8 only for the period after the fourth bore is open.

Discussion

- Mobile concentration measurements in this paper can be a promising and useful method/dataset for testing, improving existing emission models when traffic and fleet information are readily available.
- For the application in this paper, further work will focus on improving the derivation of baseline emission rates and extending the transport modeling to predict absolute (rather than relative) emission rates.



Thank you