



Yale 耶鲁大学-南京信息工程大学大气环境中心
Yale-NUIST Center on Atmospheric Environment

Spatial variations of transfer coefficients of heat, water vapor and momentum across Lake Taihu

Wei Xiao

Video conference on April 27, 2012

Outline

1. Introduction
2. Theory
3. Sites and instruments
4. Results
5. Discussion

1. Introduction

- Lake is an important land surface type for atmospheric research. The inclusion of lakes in numerical weather prediction (NWP) and climate models improves model performance. A critical issue here concerns the accuracy of the **transfer coefficients** because any bias in them will propagate directly to the flux variables.
 - To identify spatial variations of transfer coefficients of heat, water vapor and momentum across Lake Taihu;
 - To compare the transfer coefficients of Lake Taihu with physical ocean parameterization.

(Rouse et al. 2003, 2005; Long et al. 2007; Downing et al. 2006; Herderson-Sellers 1986; Bonan 1995; Betts and Ball 1997; Liu et al. 2005).

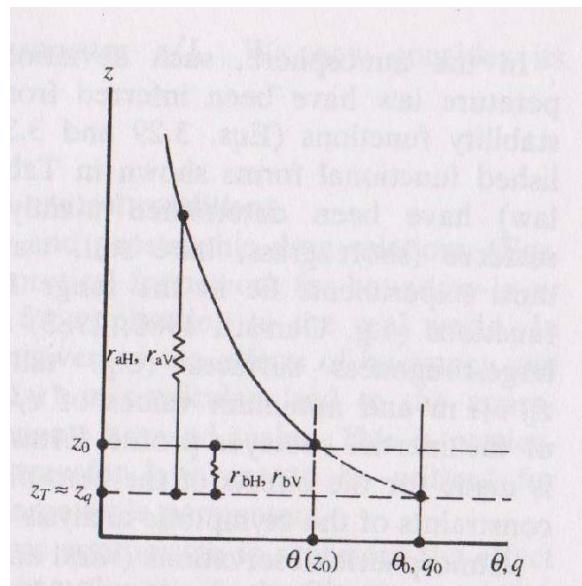
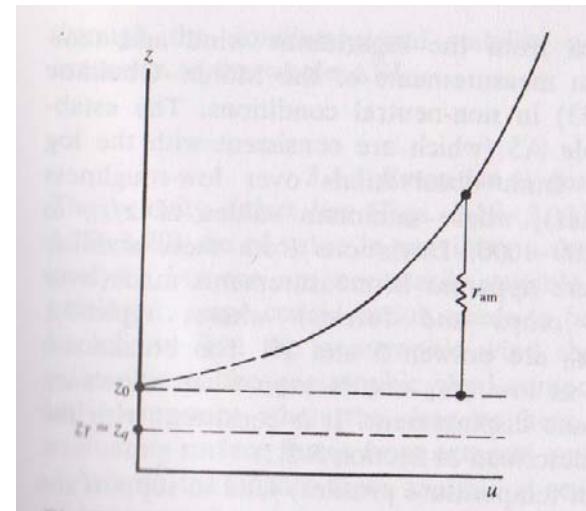
2. Theory

2.1 ROUGHNESS LENGTH VS TRANSFER COEFFICIENTS

Roughness length

- **Aerodynamic roughness length (z_0)** is a parameter of some vertical wind profile equations that model the horizontal mean wind speed near the ground; in the log wind profile, it is equivalent to the height at which the **wind speed** theoretically becomes **zero**.

$$ku / u_{*0} = \ln(z / z_0)$$



- **Scalar roughness length:** the surface-layer temperature and humidity profiles are defined in the equations with scalar roughness lengths z_T and z_q replacing z_0 in the wind profile relation.

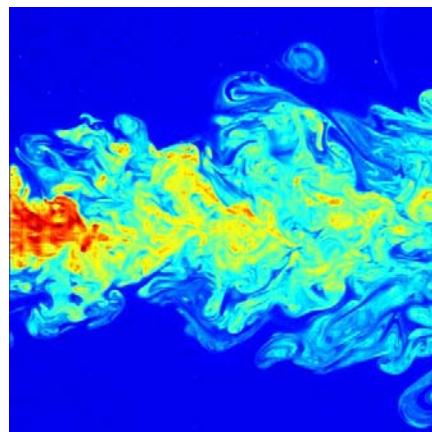
$$k(q - q_0) / q_{*0} = \ln(z / z_q) - \Psi_w(\zeta)$$

$$k(\theta_v - \theta_0) / \theta_{v*0} \approx \ln(z / z_T) - \Phi_H(\zeta)$$

Aerodynamic vs scalar roughness length

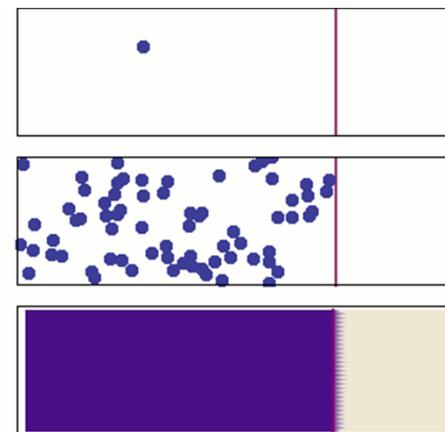
Conceptually, the distinction between z_T , z_q and z_0 is suggested by the consideration of **transport mechanisms** for heat, water vapour and momentum in the presence of aerodynamically rough flow close to the surface.

Turbulence



The transfer of **momentum** is effected by **pressure fluctuations** in the turbulent wakes behind the roughness elements.

Molecular diffusion



Heat and water vapour must ultimately be transferred by **molecular diffusion** across the interfacial sublayer.

Transfer coefficients - the surface roughness

$$C_{DN} = k^2 / [\ln(z/z_0)]^2$$

Momentum roughness

$$C_{EN} = k^2 / [\ln(z/z_0) \ln(z/z_q)]$$

Roughness length for water vapor

$$C_{HN} = k^2 / [\ln(z/z_0) \ln(z/z_T)]$$

Roughness length for temperature

The neutral transfer coefficients at the height of 10 m above the water surface

$$C_{D10N} = k^2 / [\ln(10/z_0)]^2$$

$$C_{E10N} = k^2 / [\ln(10/z_0) \ln(10/z_q)]$$

$$C_{H10N} = k^2 / [\ln(10/z_0) \ln(10/z_T)]$$

Mass transfer equations

Momentum flux

$$\tau = \rho_a C_D u^2$$

Drag coefficient

Latent heat flux

$$LE = \rho_a L_v C_E u (q_s - q_a)$$

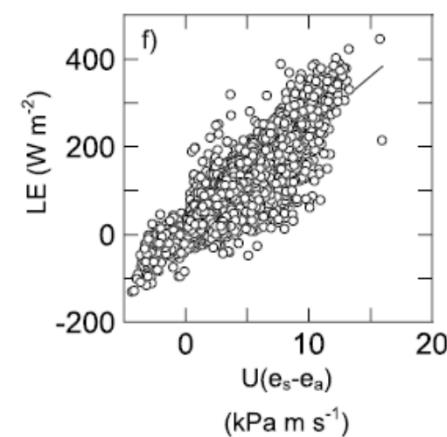
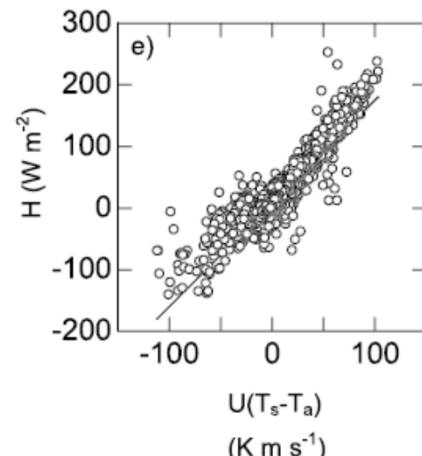
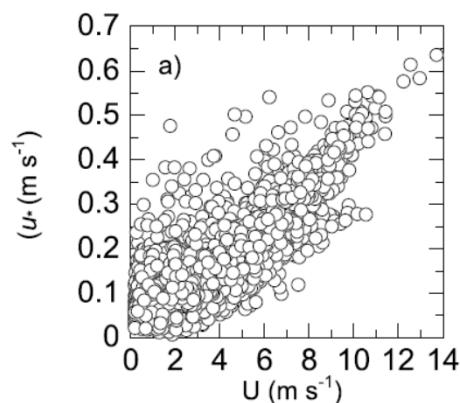
Transfer coefficient for moisture

Sensible heat flux

$$H = \rho_a c_p C_H u (\theta_s - \theta_a)$$

Transfer coefficient for heat

The coefficients C_{DN} , C_{EN} and C_{HN} were optimized by minimizing the bias between the observation and calculation of τ , LE and H .



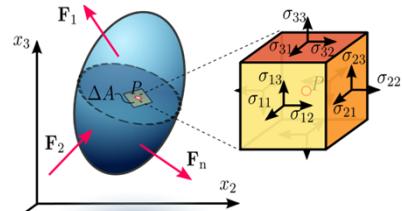
(Liu et al. 2009)

2. Theory

2.2 GARRATT/BRUTSAERT MODEL

Smooth vs Rough surface over water

Shear stress



Turbulent boundary layer

Viscous sublayer δ_1

Smooth surface

Aerodynamically rough surface

$$h_r \gg \delta_1$$

$$u_* h_r / v > 75$$

Aerodynamically smooth surface

$$h_r \ll \delta_1$$

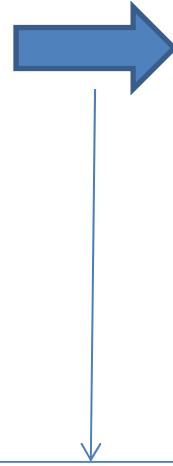
$$u_* h_r / v < 5$$

h_r – the height of the roughness elements

- Aerodynamically smooth:
 $Re_* \approx 0.11$



- Fully rough:
 $Re_* > 2$



- **Wave breaking:** a transfer of energy from the already saturated wave components (ripples) to turbulence.
- $Re_* \approx 2, u_{*0} \approx 0.23 \text{ m s}^{-1}$ ($u_{10} \approx 5.5 \text{ m s}^{-1}$)

The aerodynamic roughness length over sea

- In very light winds --> aerodynamically smooth surface

$$z_0 \approx 0.11v/u_{*0}$$

- In rough flow conditions

$$z_0 = \alpha_c u_{*0}^2 / g$$

$$z_0 = (\alpha_c u_{*0}^2 / g) (\mu_w u_{*0} / \sigma_t)^{m-2}$$

Drag coefficients over sea

Aerodynamically smooth flow

$$C_{DN} = k^2 / [\ln(u_{*0}z / 0.11v)]^2$$

Rough flow

$$C_{DN} = k^2 / [\ln(zg / \alpha_c u_{*0}^2)]^2$$

Transitional regime: $2.5 < u_{10} < 5.5 \text{ /s}$

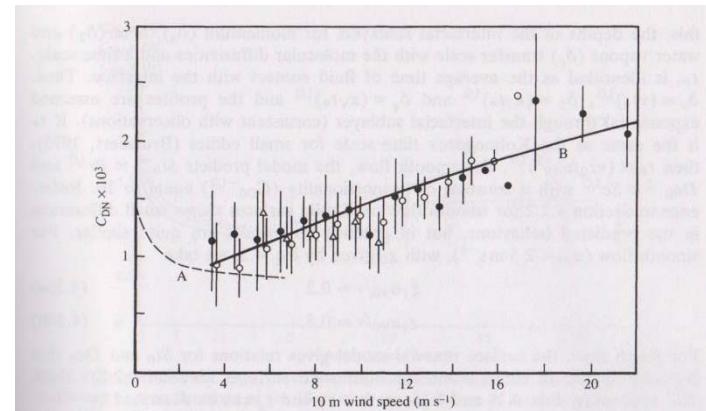


Fig. 4.8 Neutral drag coefficient over the sea as a function of the 10 m wind speed based on individual data taken from the literature. Data points represent many single runs (between 3 and 84) with the root-mean-square variation also shown. Curve A, for smooth flow, represents Eq. 4.3, and curve B, for rough flow, represents Eq. 4.5 ($\alpha_c = 0.016$). After Garratt (1977a), *Monthly Weather Review*, American Meteorological Society.

Bulk parameterization for heat transfer

$$C_{HN} = C_{DN}^{1/2} / (B_H^{-1} + C_{DN}^{-1/2})$$

$$B_H^{-1} = St_0^{-1} - C_{D0}^{-1/2} = k^{-1} \ln(z_0 / z_T)$$

For smooth flow

$$z_T u_{*0} / \nu \approx 0.2$$

For fully rough flow

$$\ln(z_0 / z_T) = 2.48 Re_*^{1/4} - 2$$

$$Re_* = u_{*0} z_0 / \nu$$

Bulk parameterization for water vapor transfer

$$C_{EN} = C_{DN}^{1/2} / (B_V^{-1} + C_{DN}^{-1/2})$$

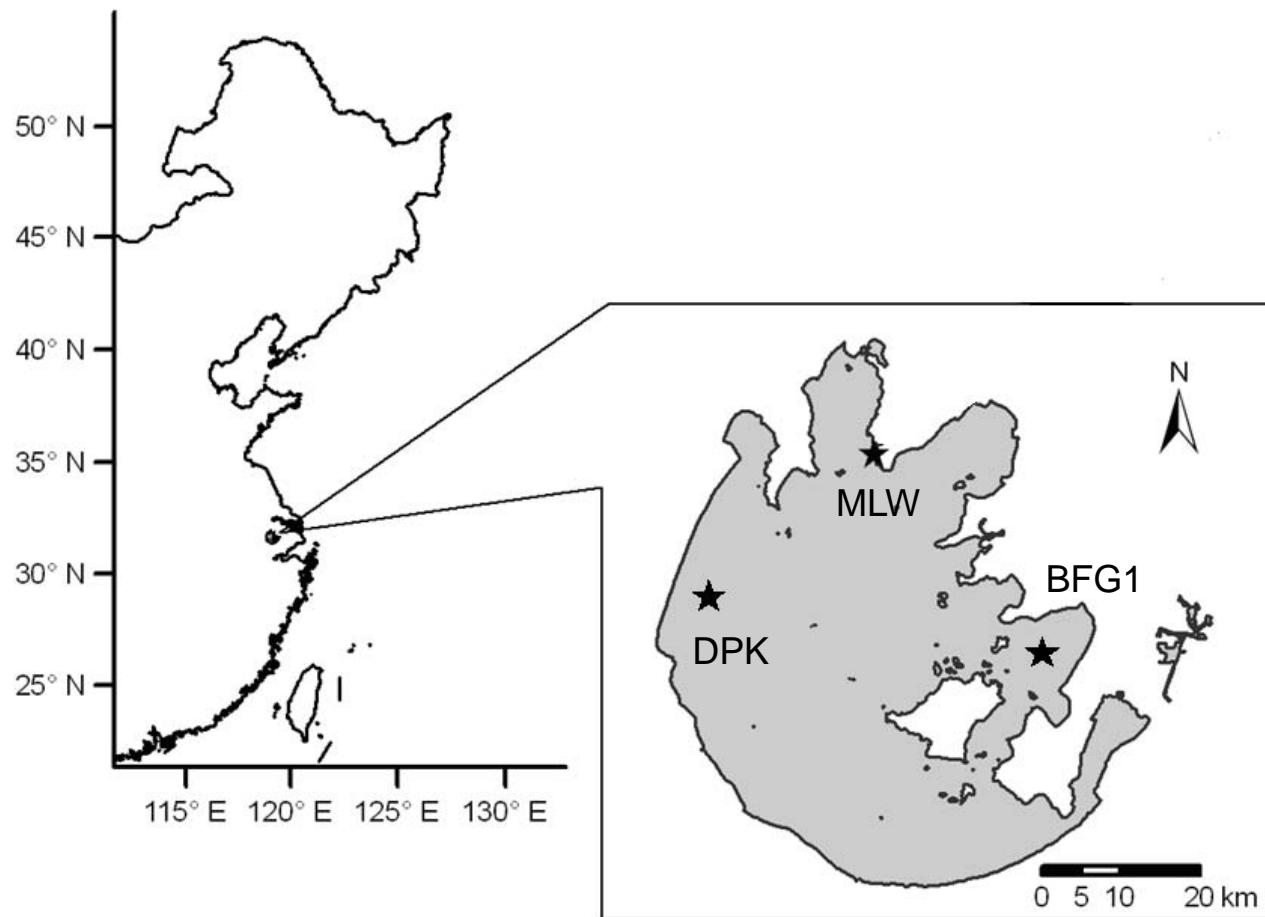
$$B_V^{-1} = Da_0^{-1} - C_{D0}^{-1/2} = k^{-1} \ln(z_0 / z_q)$$

smooth flow $z_q u_{*0} / \nu \approx 0.3$

rough flow $\ln(z_0 / z_q) = 2.28 Re_*^{1/4} - 2$

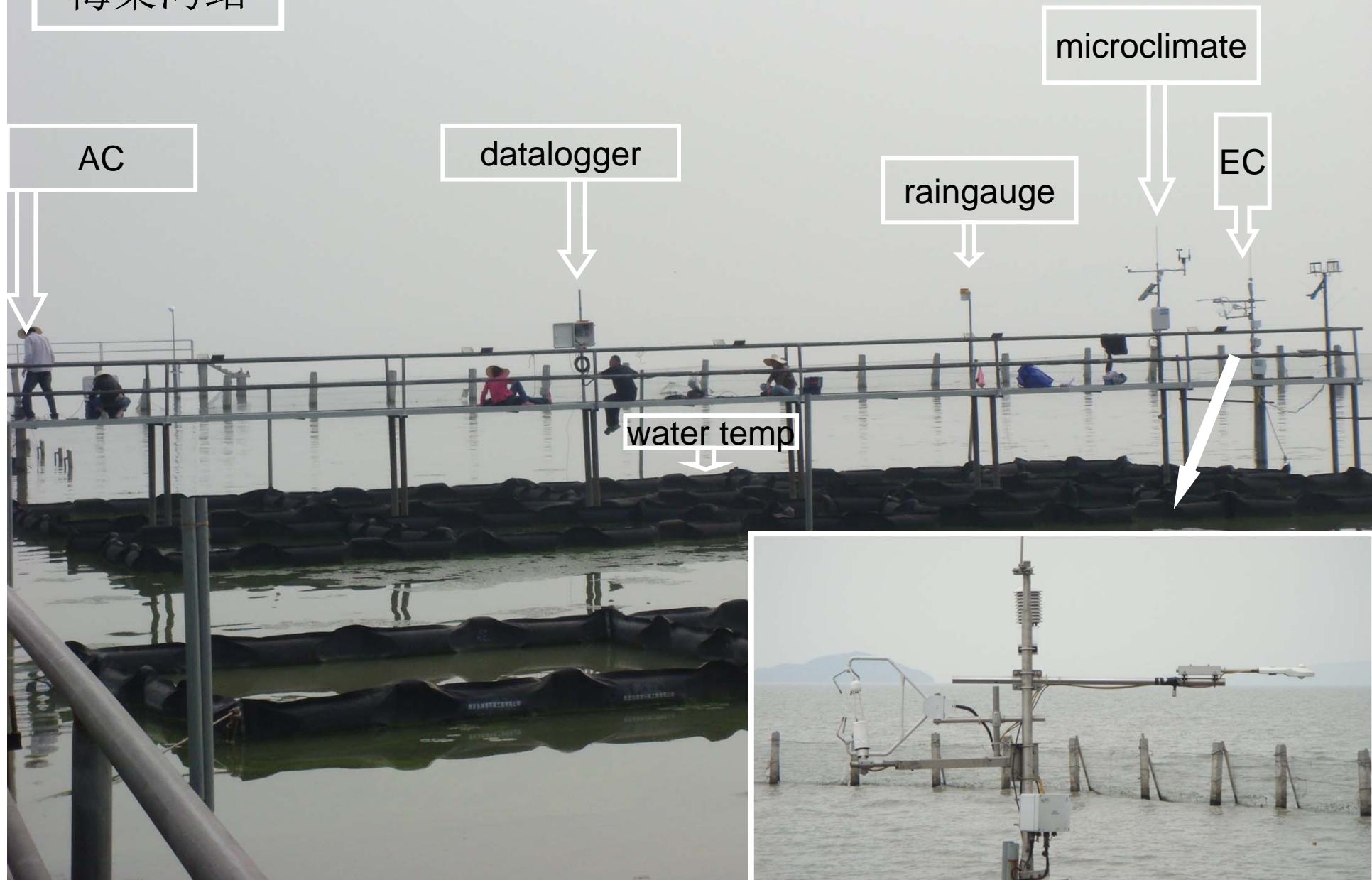
$$Re_* = u_{*0} z_0 / \nu$$

3. Sites and instruments



MLW site
梅梁湾站

Wind direction: 200-315°



DPK site
大浦口站



Wind direction: 100-280°

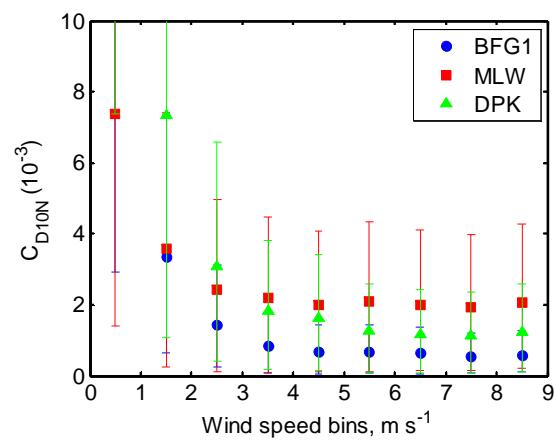
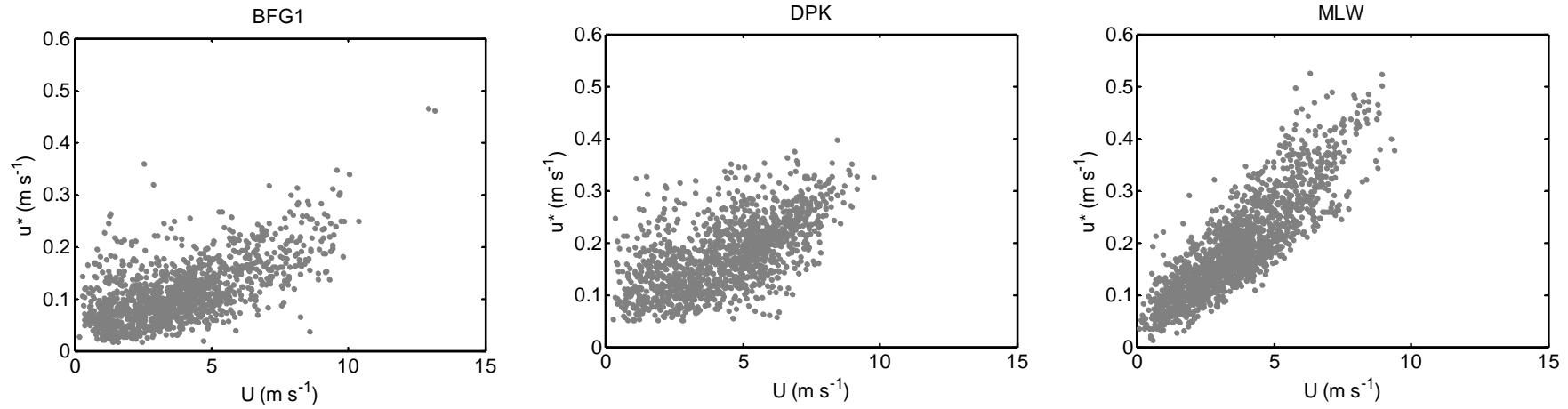
Wind direction: 135-315°



BFG1 site
1号避风港

4. RESULTS

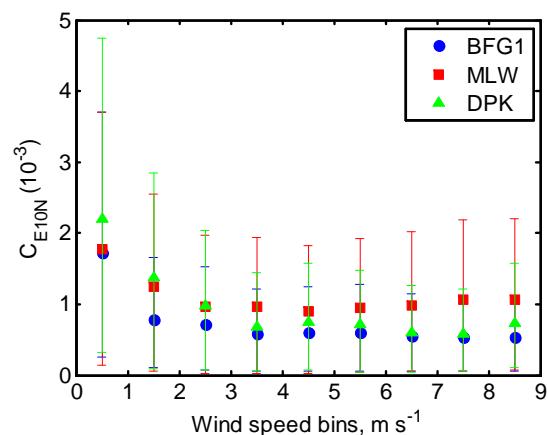
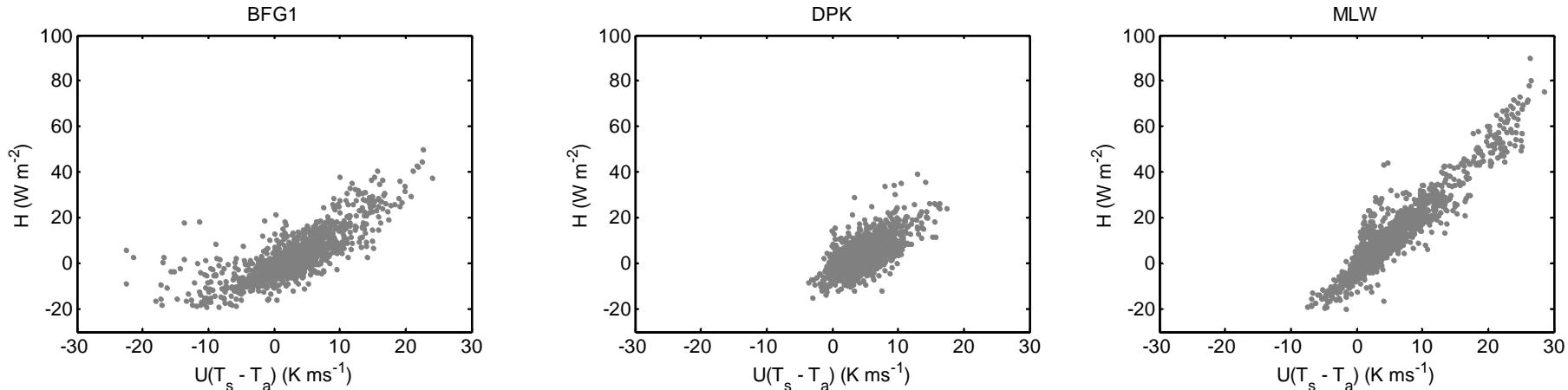
Drag coefficients



MLW > DPK > BFG1

$10^3 C_{D10N}$	BFG1	DPK	MLW
$u < 1$	12.05	19.62	7.36
$1 < u < 2$	3.34	7.34	3.58
$2 < u < 3$	1.44	3.08	2.42
$3 < u < 4$	0.84	1.82	2.19
$4 < u < 5$	0.69	1.64	1.99
$5 < u < 6$	0.68	1.26	2.11
$6 < u < 7$	0.65	1.18	1.99
$7 < u < 8$	0.56	1.15	1.92
$8 < u < 9$	0.59	1.23	2.05

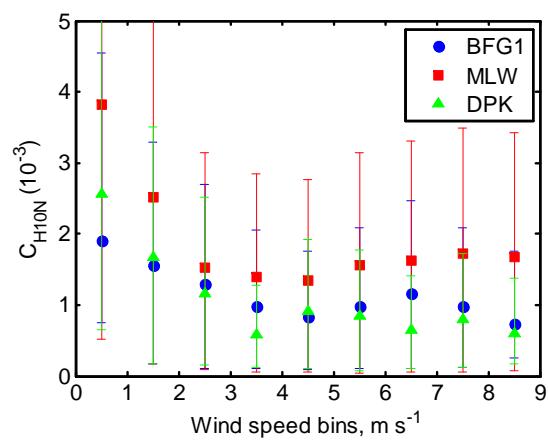
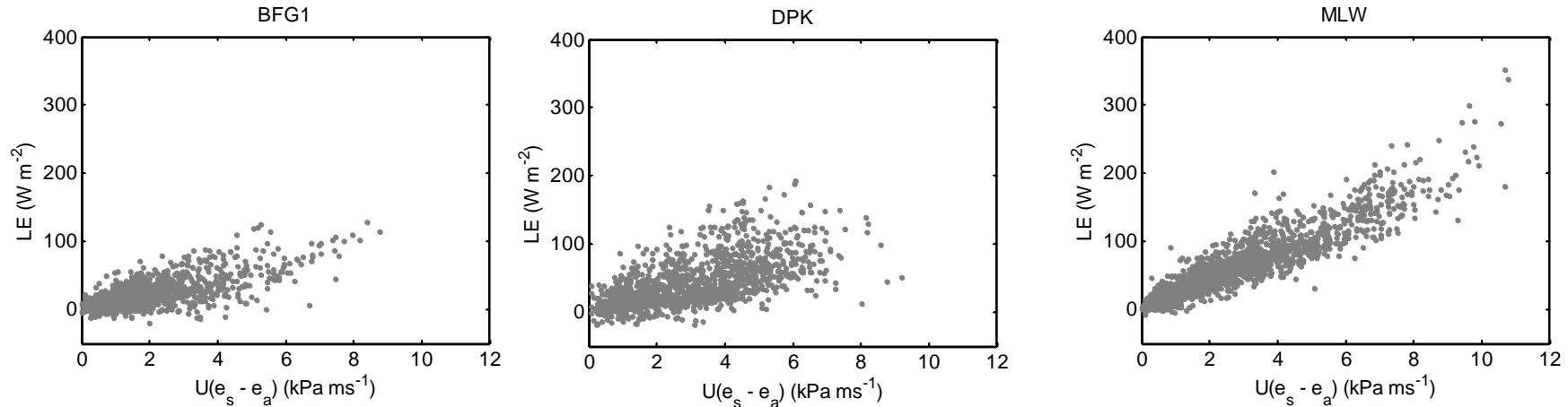
Heat transfer coefficients



MLW > BFG1 > DPK

$10^3 C_{H10N}$	BFG1	DPK	MLW
$u < 1$	1.90	2.56	7.36
$1 < u < 2$	1.56	1.67	3.58
$2 < u < 3$	1.29	1.17	2.42
$3 < u < 4$	0.98	0.58	2.19
$4 < u < 5$	0.83	0.92	1.99
$5 < u < 6$	0.99	0.85	2.11
$6 < u < 7$	1.17	0.66	1.99
$7 < u < 8$	0.98	0.80	1.92
$8 < u < 9$	0.74	0.60	2.05

Water vapor transfer coefficients



$\text{MLW} > \text{BFG1} > \text{DPK}$

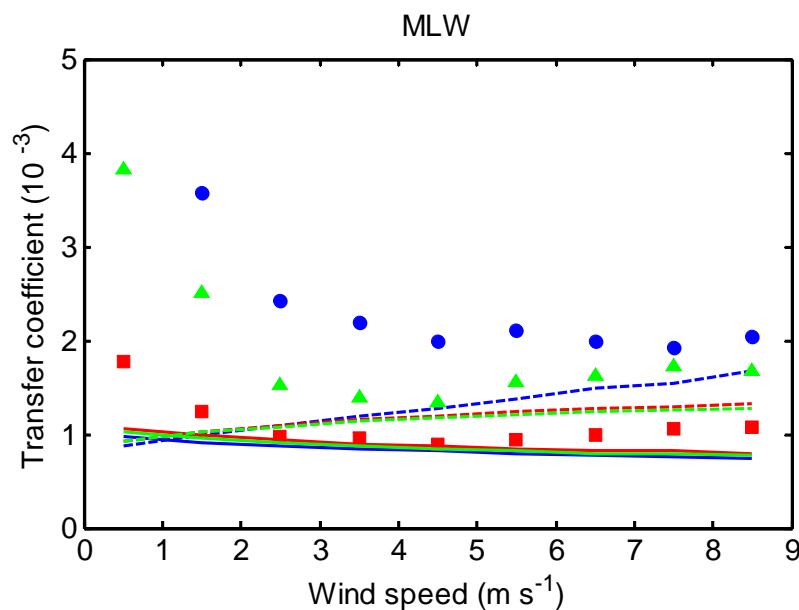
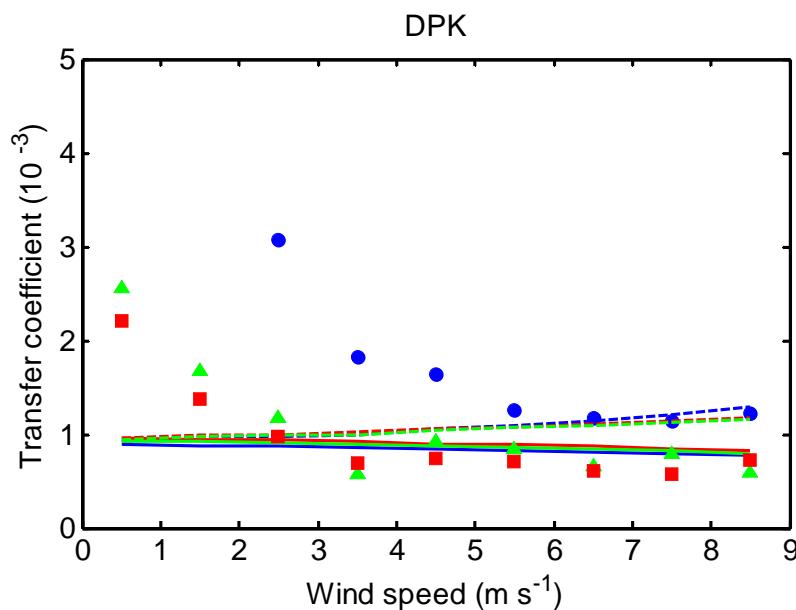
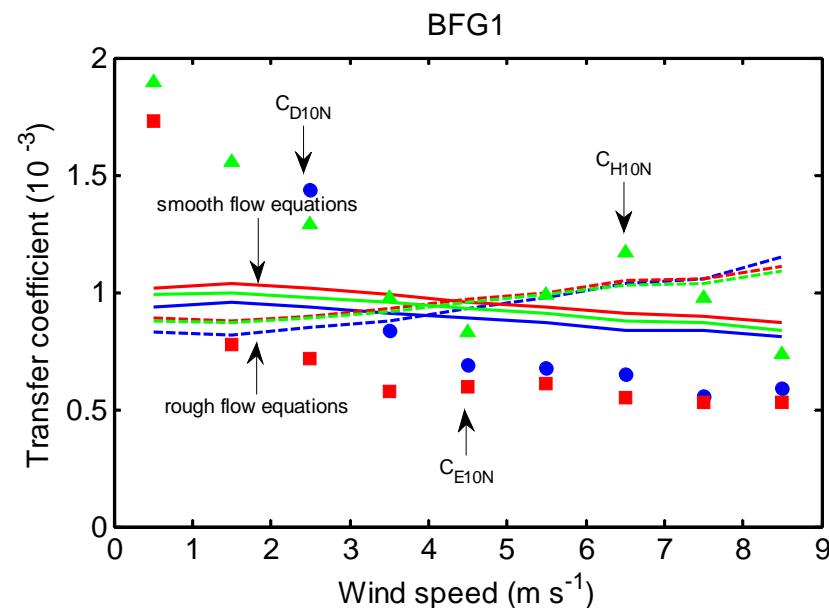
$10^3 C_{E10N}$	BFG1	DPK	MLW
$u < 1$	1.73	2.21	1.78
$1 < u < 2$	0.78	1.38	1.25
$2 < u < 3$	0.72	0.98	0.97
$3 < u < 4$	0.58	0.69	0.96
$4 < u < 5$	0.60	0.75	0.90
$5 < u < 6$	0.61	0.71	0.95
$6 < u < 7$	0.55	0.61	0.99
$7 < u < 8$	0.53	0.58	1.06
$8 < u < 9$	0.53	0.73	1.07

Garratt's model versus optimization results

BFG1: $C_{H10N} > C_{D10N} > C_{E10N}$

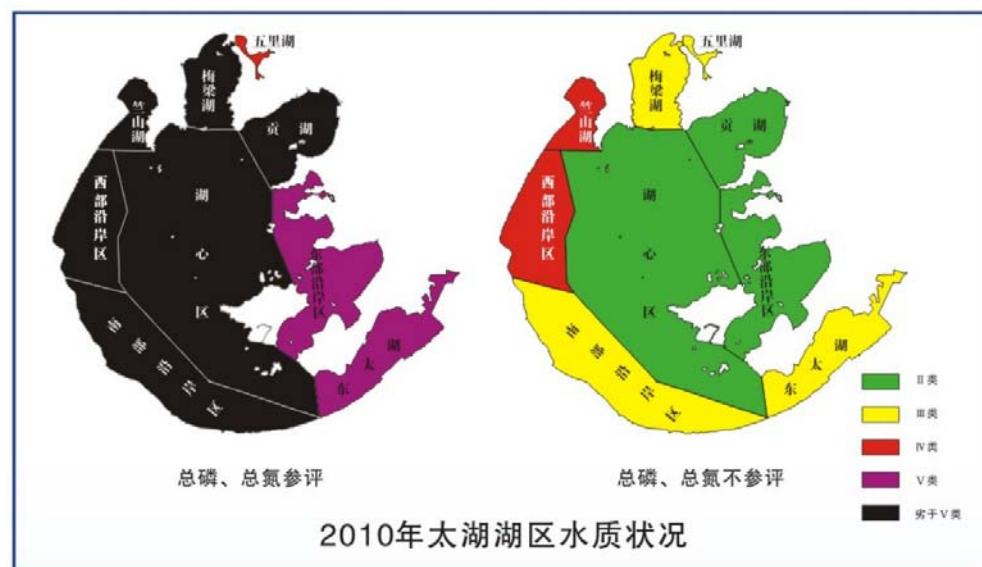
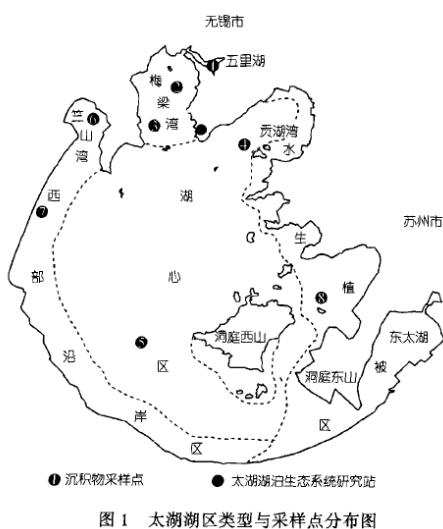
DPK: $C_{D10N} > C_{H10N} \sim C_{E10N}$

MLW: $C_{D10N} > C_{H10N} > C_{E10N}$



5. Discussion

- Low wind speed: how to identify the transfer coefficients?
- What drives the spatial variation of transfer coefficient on Lake Taihu? Fetch, depth, or submerged vegetation?

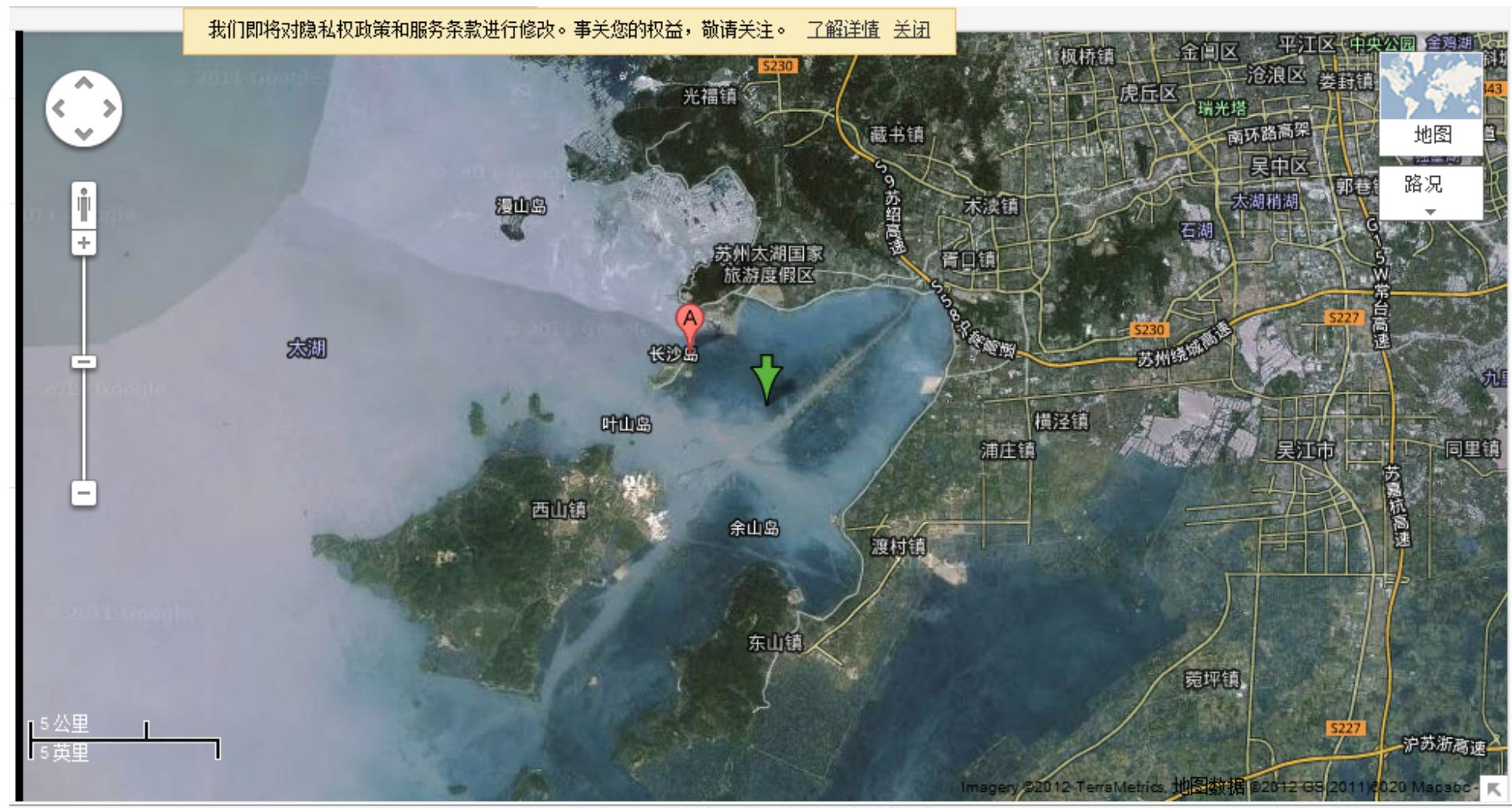


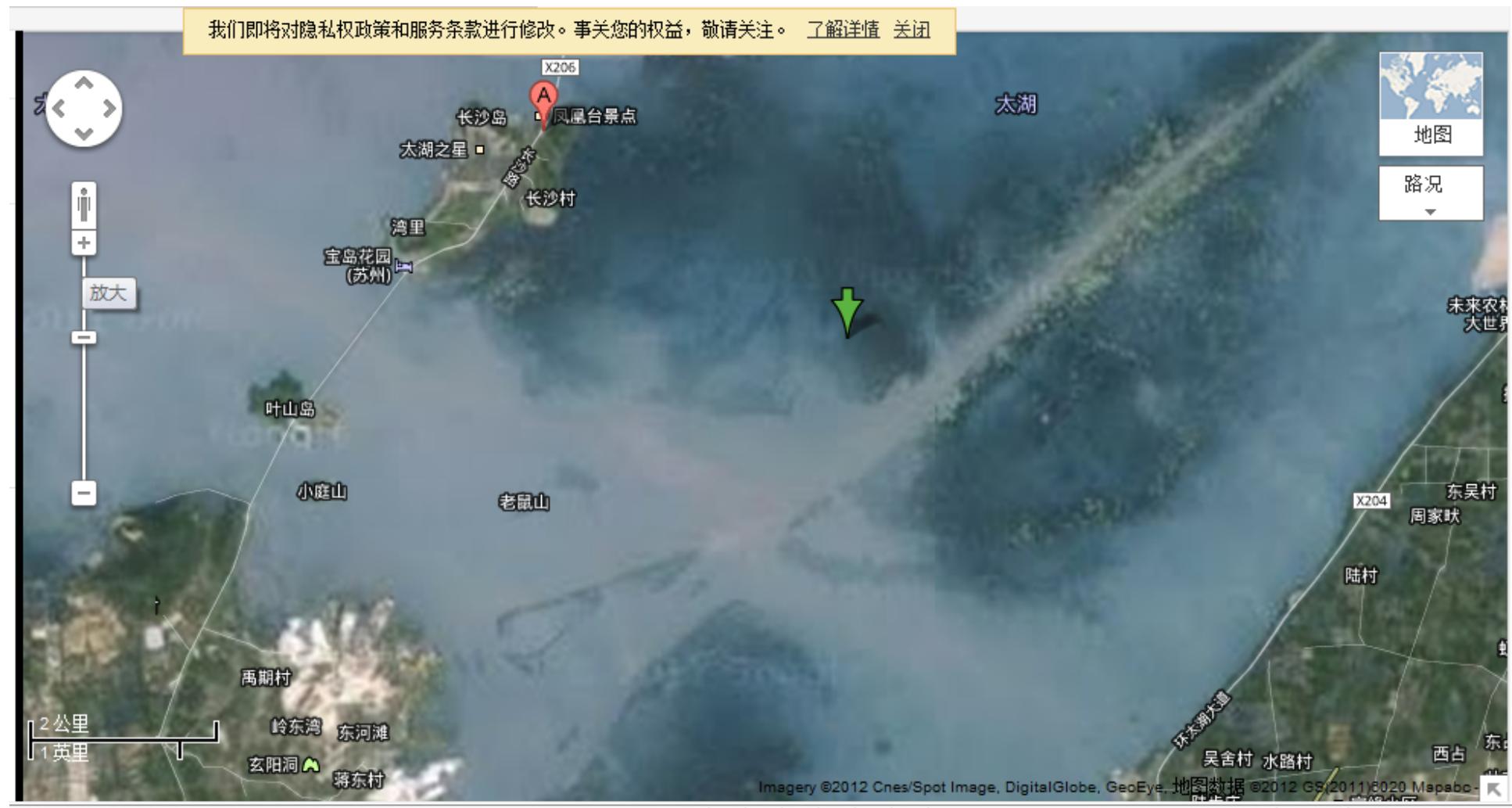
BFG1(1号避风港)通量站

Location: 120° 24'01"E, 31° 10'28"N

Started from: December 15, 2011



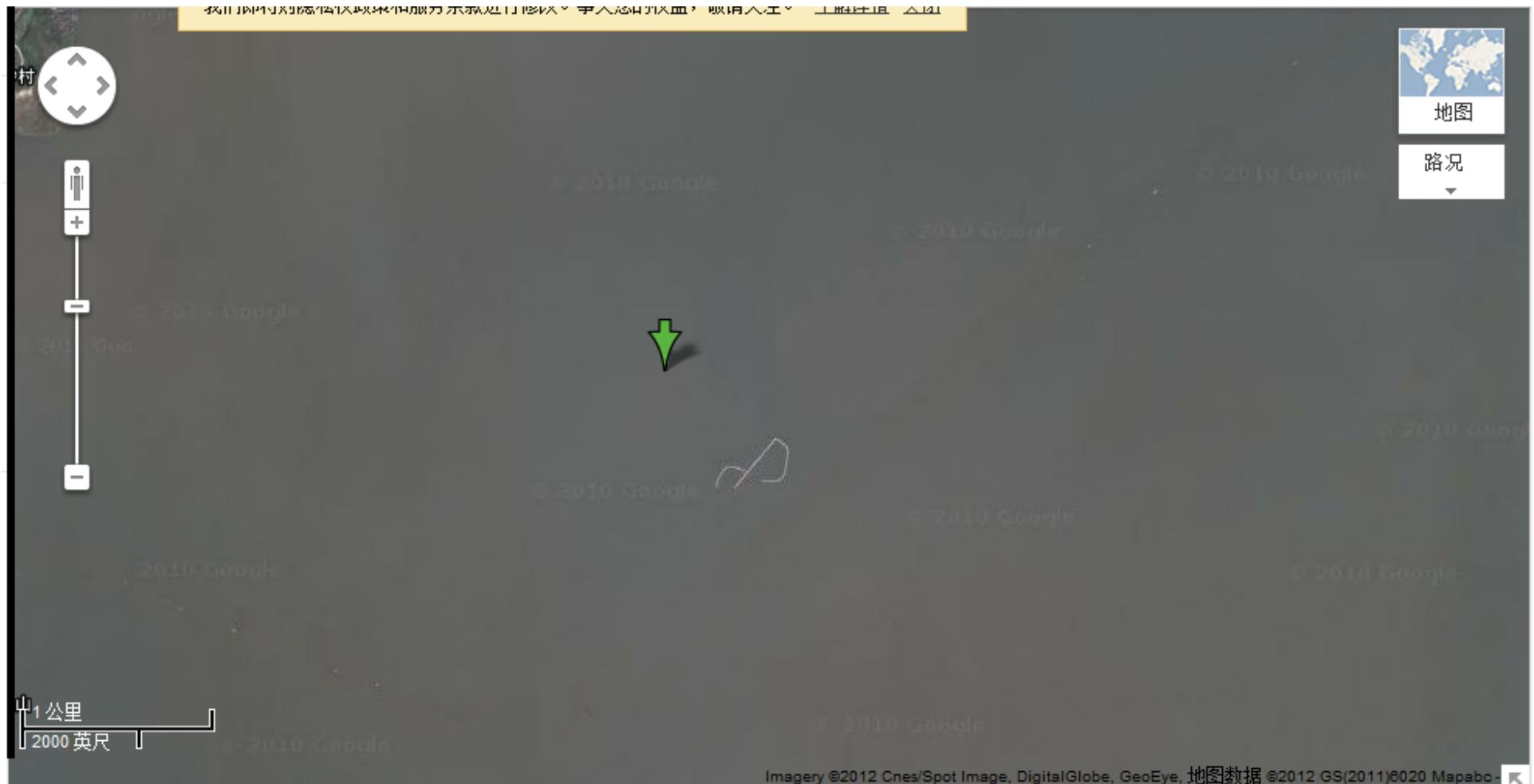


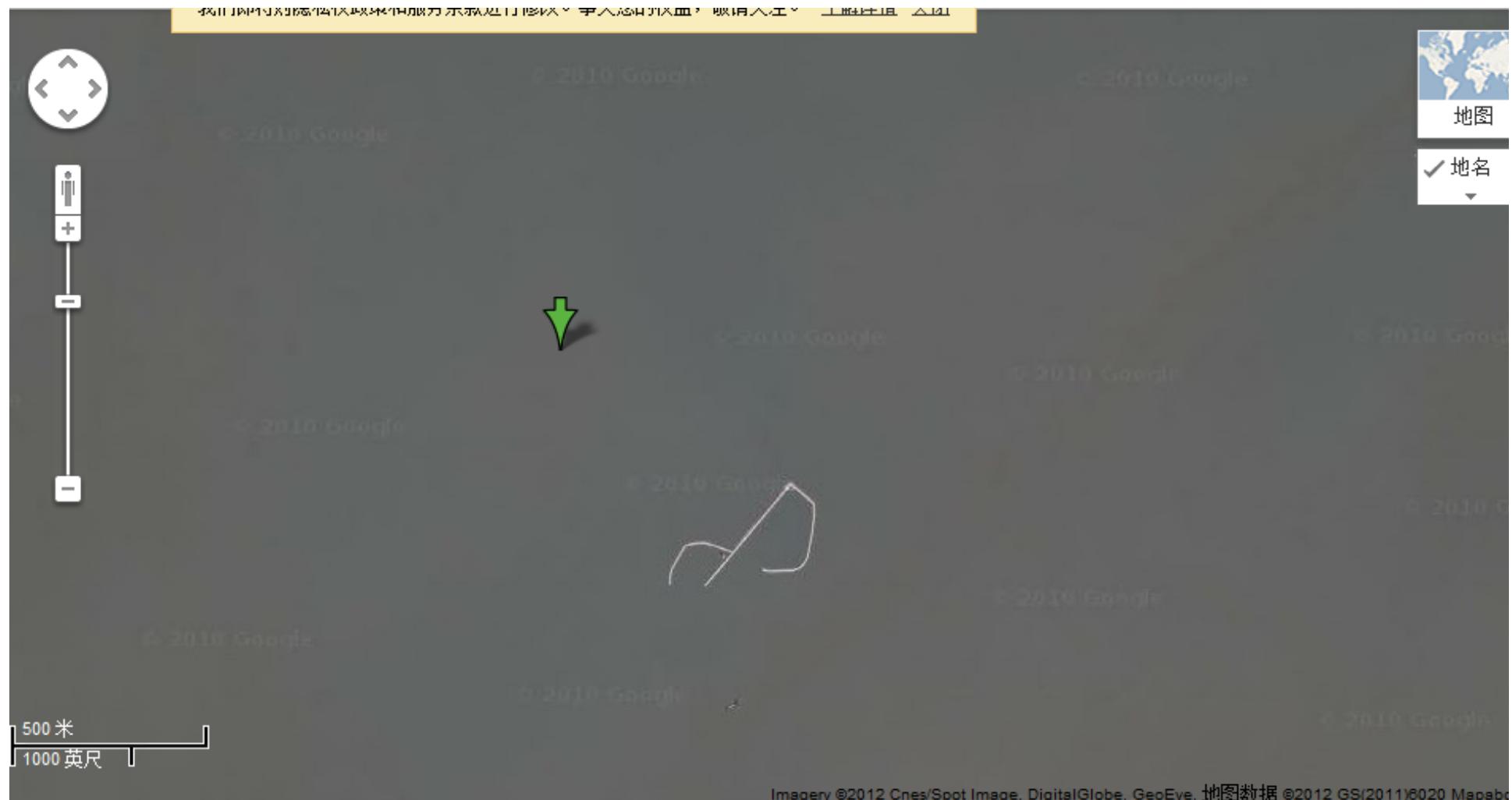


3km

我们即将对隐私权政策和服务条款进行修改。事关您的权益，敬请关注。[了解详情](#) [关闭](#)



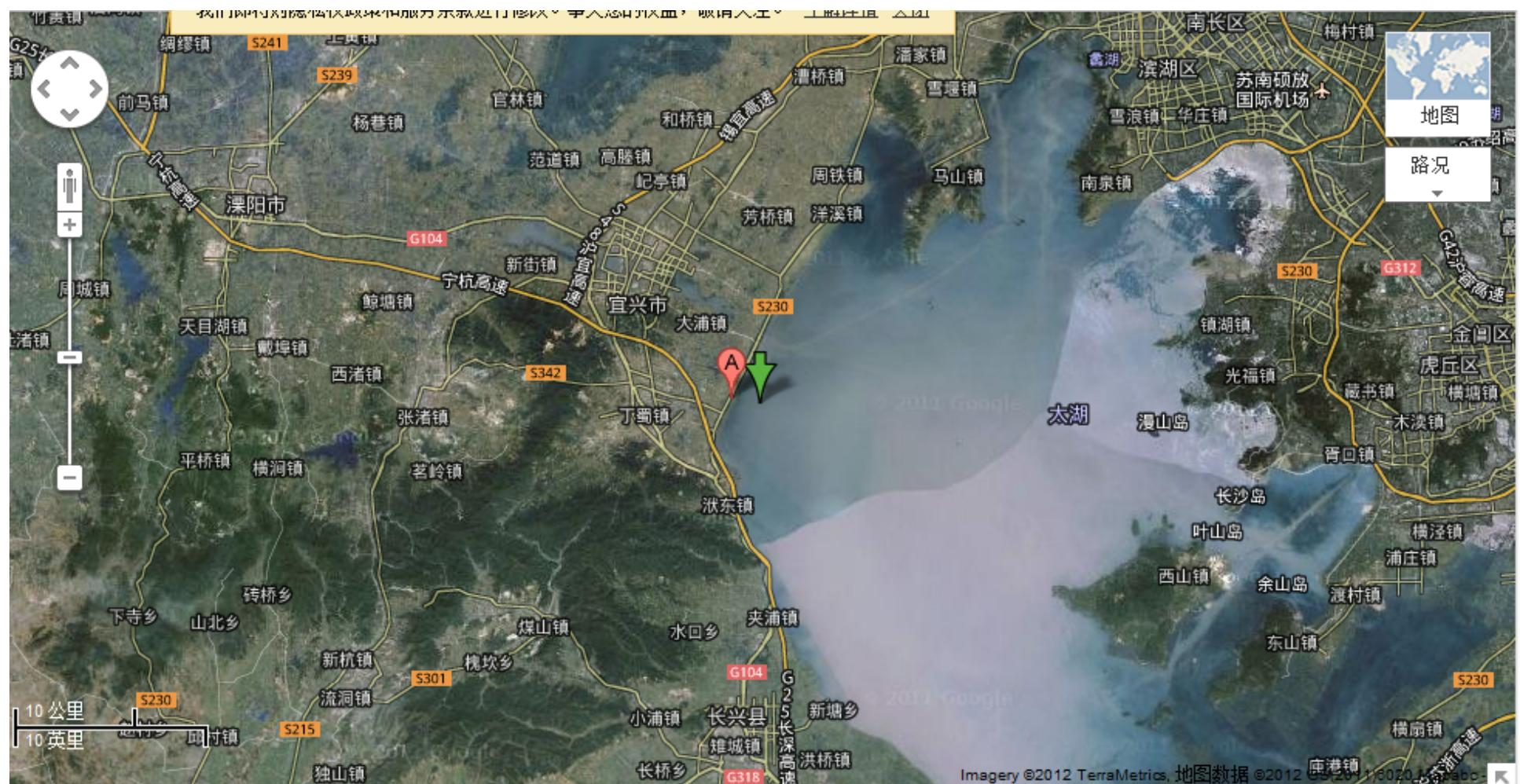


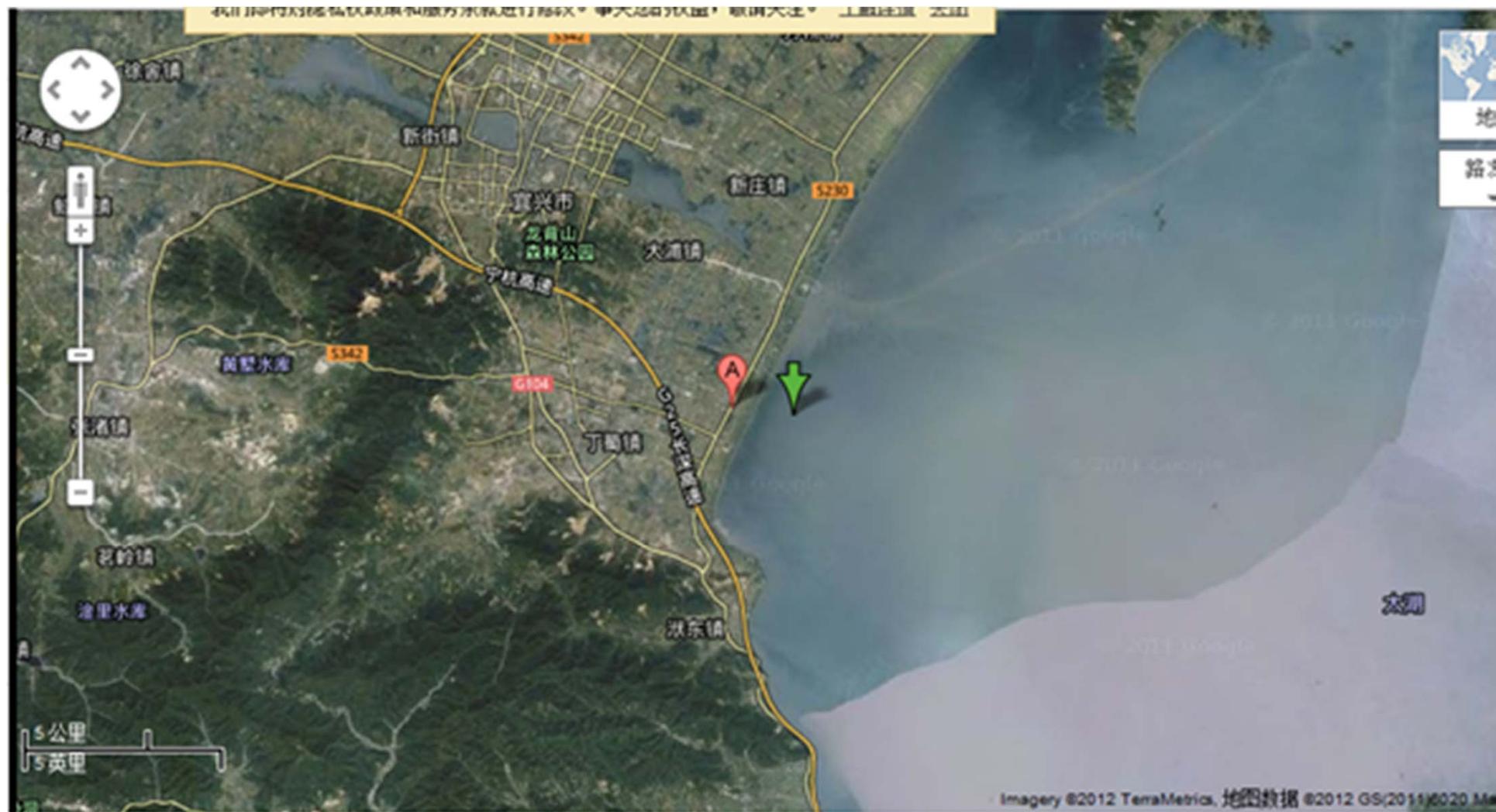


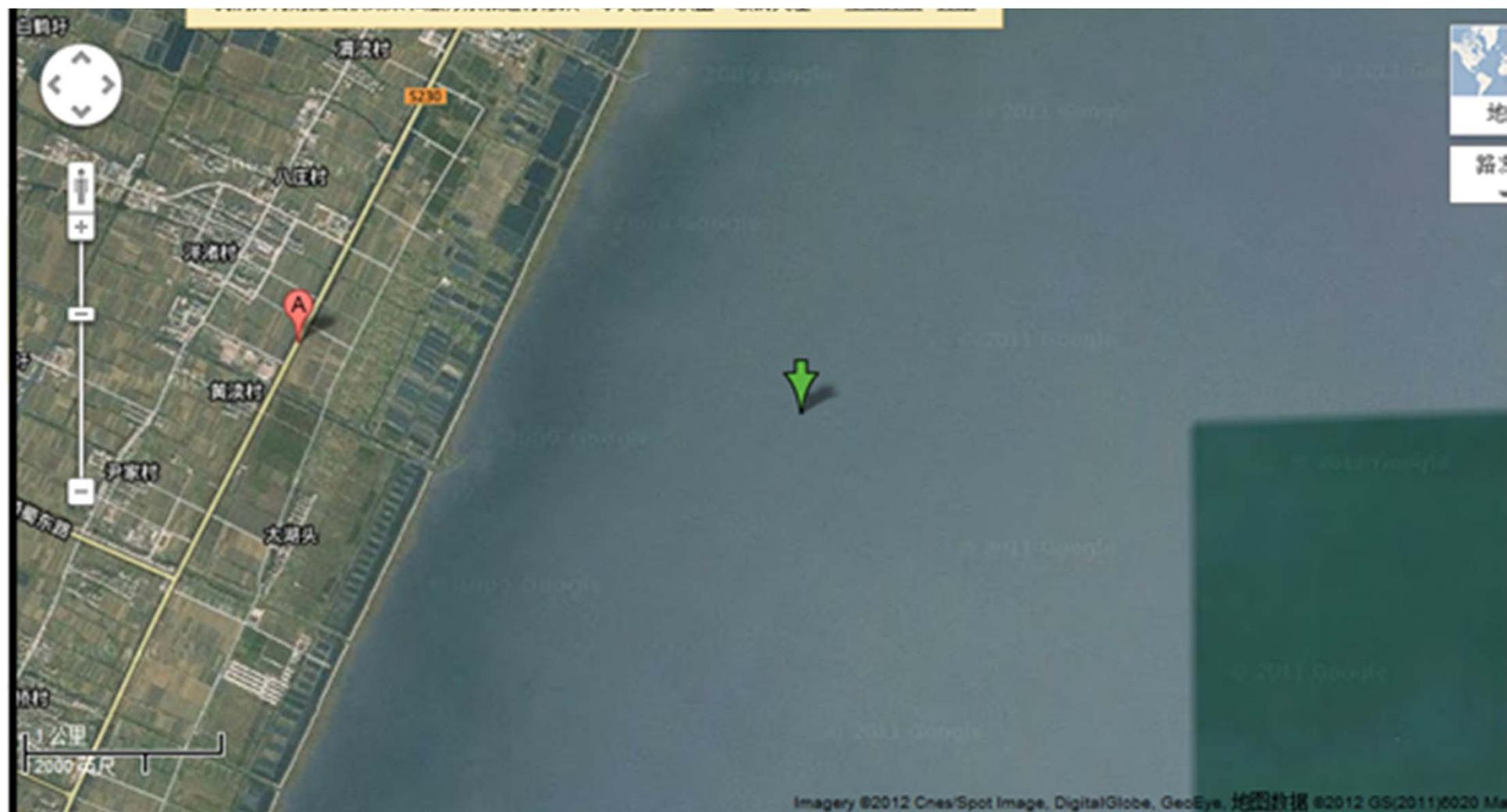
600m

Description of Dapukou(DPK, 大浦口) flux site

- Radiation measurement was started on December 3, 2010
- Eddy covariance, meteorology & water temperature was started from August 17, 2011
- Location: $119^{\circ} 55'52.3"E, 31^{\circ} 15'57.8"N$







1.5km

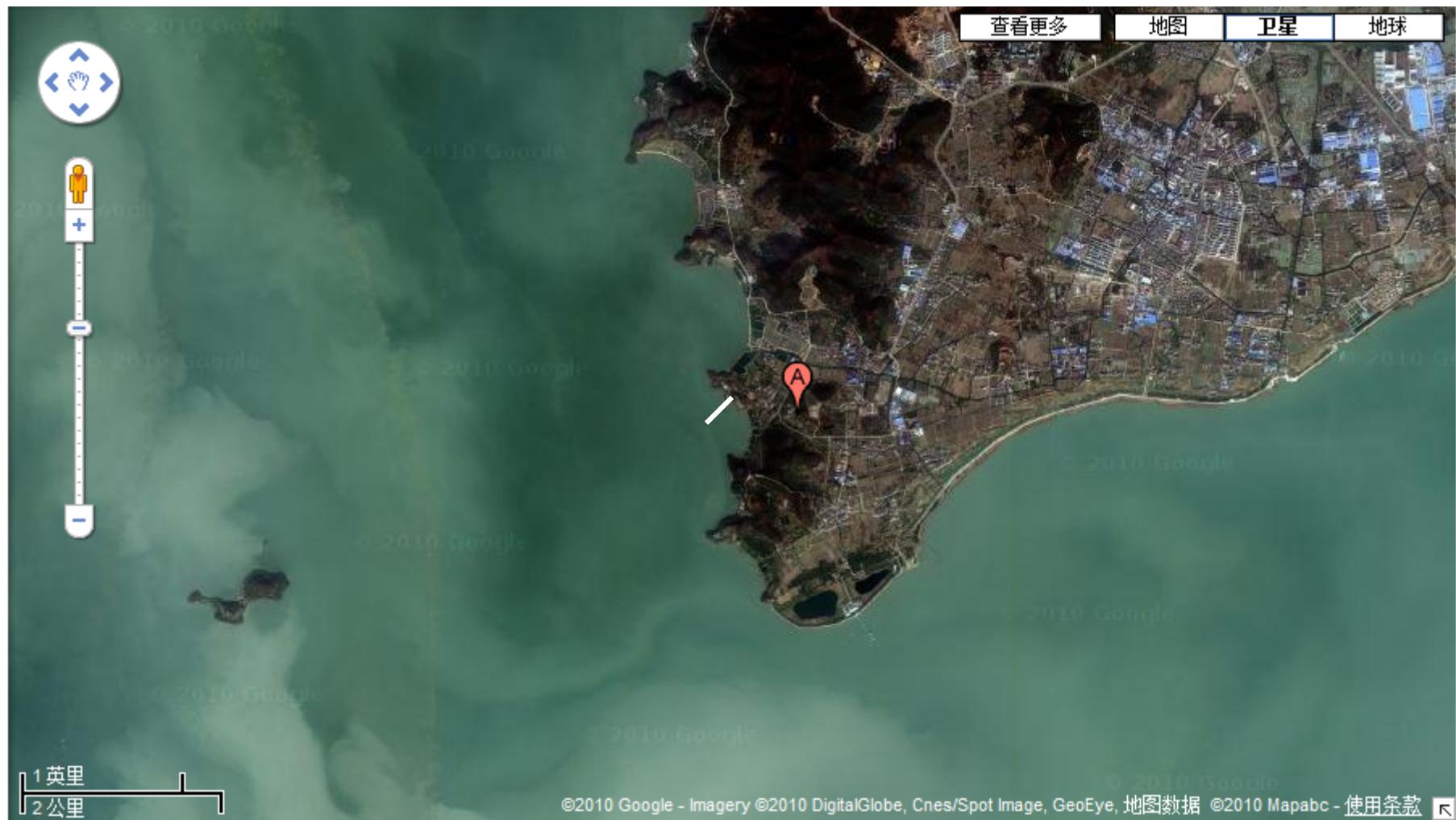
MLW (梅梁湾) site description

Location: 31° 24'N, 120° 13'E



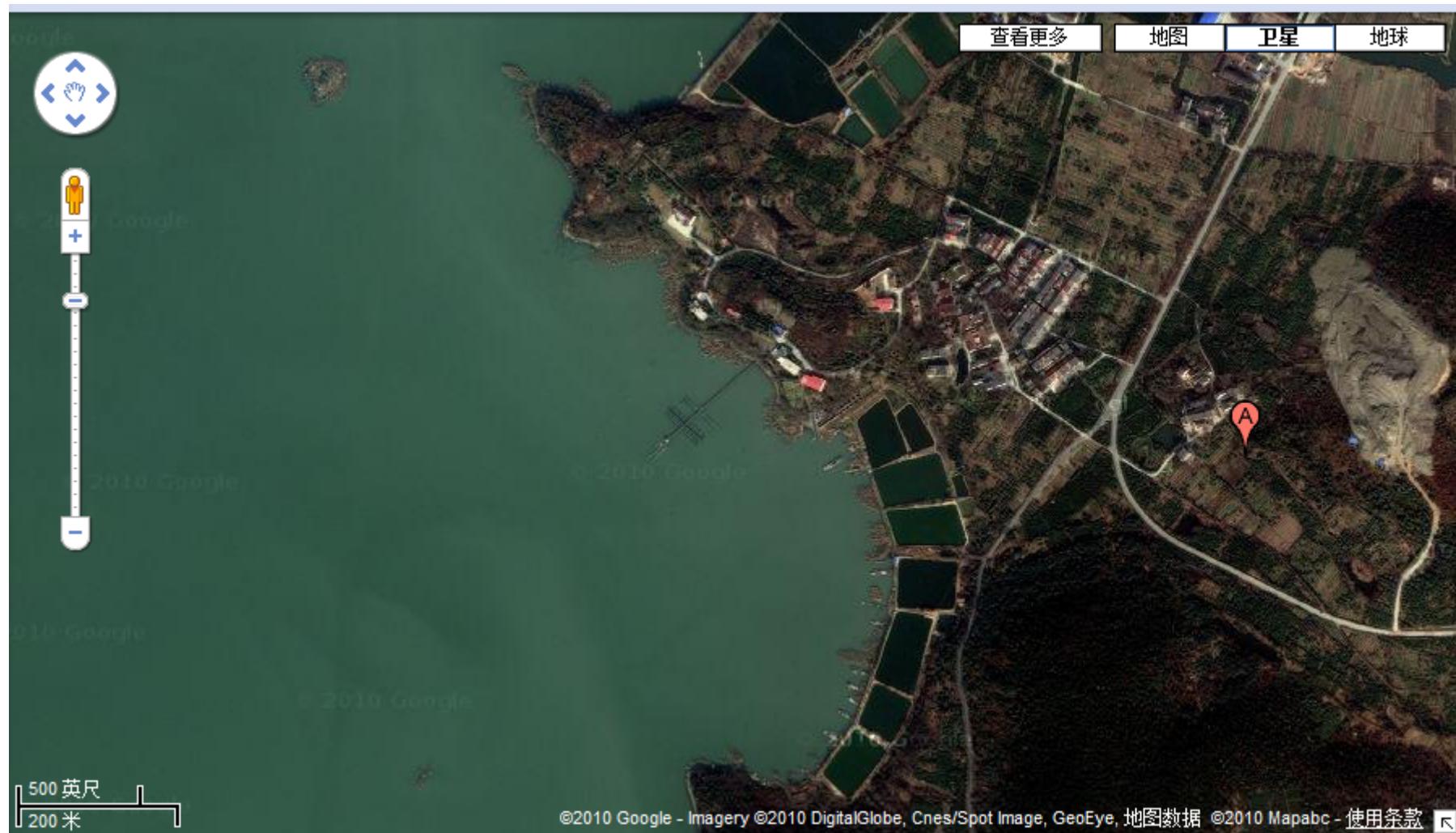


Our Experimental Site

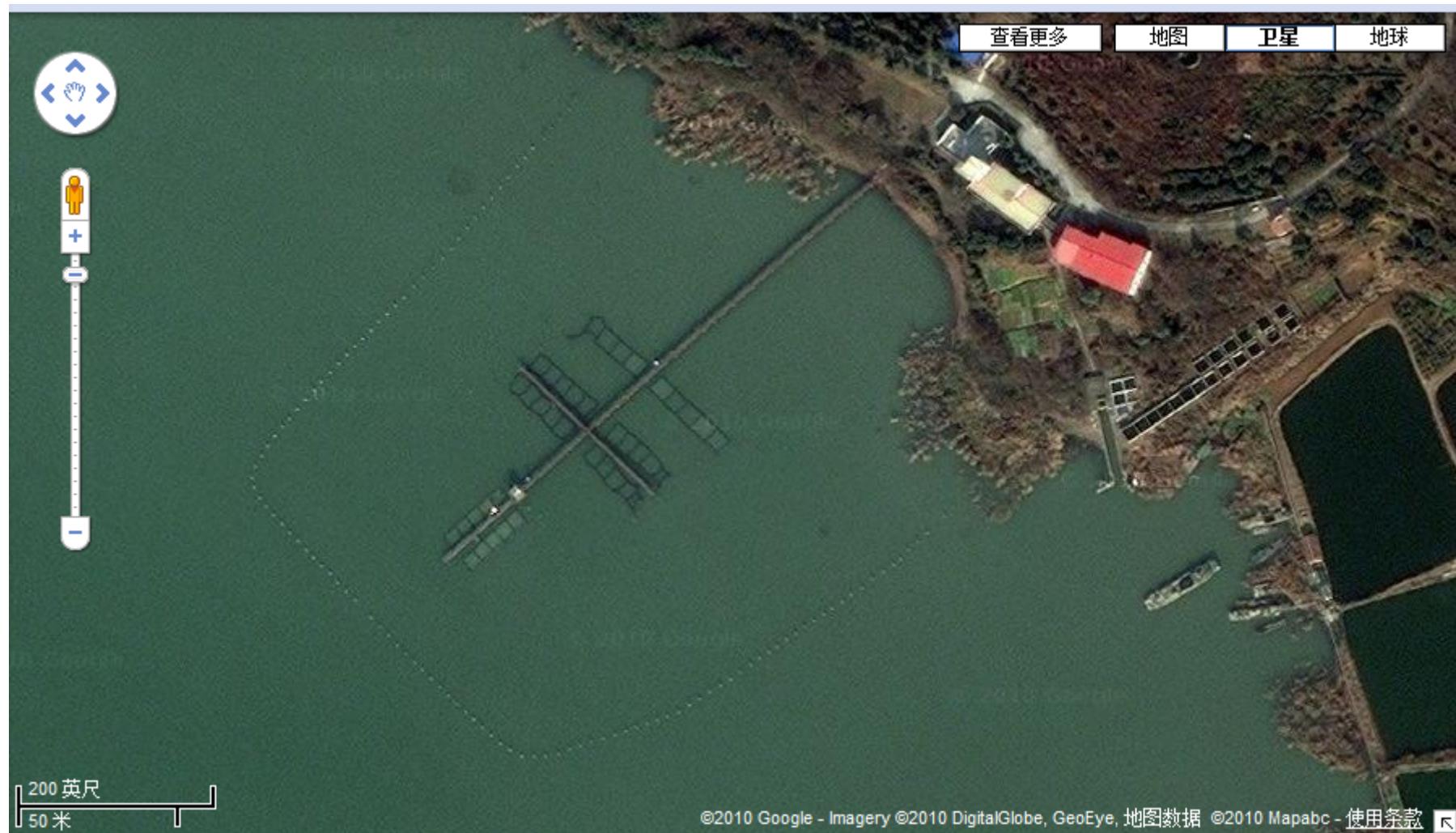


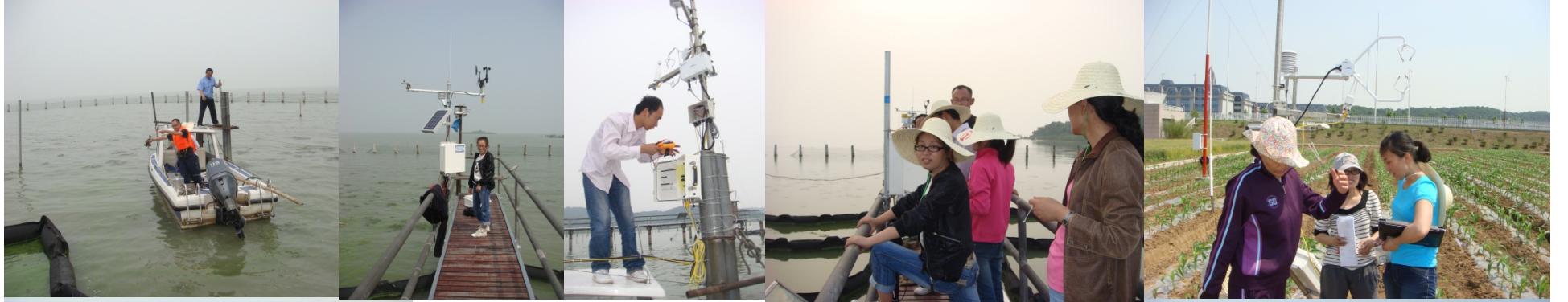
Good fetch: 180~315° south and west wind

Our Experimental Site



Our Experimental Site





Thank you!