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基于光谱分析仪的通量-梯度法测量小型池塘水-气界 面温室气体交换通量

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摘要:小型池塘作为内陆水体的一部分,是被忽视的温室气体重要排放源.本研究主要利用通量-梯度方法测量长江三角洲地区的一处小型池塘水-气界面温室气体 $(CO_2 \ n\ CH_4)$ 交换通量.结果表明:①零梯度测试结果显示本套通量-梯度系统测量 $H_2O_1 CO_2 \ n\ CH_4$ 通量的精度分别为 7.525 $W \cdot m^{-2} \cdot 0.022 \ mg \cdot (m^2 \cdot s)^{-1} \cdot 0.054 \ \mug \cdot (m^2 \cdot s)^{-1}$,并且在正常实验观测期间 3 种气体 $(H_2O_1 CO_2 \ n\ CH_4)$ 的通量值分别有 84%、80% 和 94% 的结果高于零梯度测试精度,以上结果可以保证本套通量-梯度系统具有足够的精度测量池塘水-气界面温室气体交换通量;②通量-梯度计算结果表明此小型池塘在夏季为 $CO_2 \ n\ CH_4$ 的排放源,其排放通量平均值分别为 0.038 $mg \cdot (m^2 \cdot s)^{-1}$ 和 0.889 $\mu g \cdot (m^2 \cdot s)^{-1}$,其中 CH_4 排放通量远高于内陆湖泊甲烷排放通量的中值,说明小型池塘的温室气体排放量是估算内陆水体温室气体排放量特别是 CH_4 排放量中不可忽视的重要量值,本研究结果可为准确估算区域温室气体排放量提供科学参考.

关键词:小型池塘;温室气体通量;水-气界面;通量-梯度方法;涡度相关方法;光谱分析仪中图分类号: X16 文献标识码: A 文章编号: 0250-3301(2017)01-0041-11 **DOI**: 10.13227/j. hjkx. 201605142

Greenhouse Gas Fluxes at Water-Air Interface in Small Pond Using Flux-Gradient Method Based on Spectrum Analyzer

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Abstract: As an important part of inland waters, small pond is a neglected source of greenhouse gas. The main objective of the study was to quantify greenhouse gas fluxes (CO_2 and CH_4) from small pond in the Yangtze Delta using flux-gradient method. The results showed that: ① zero-gradient test indicated that the flux measurement precision for water vapor, CO_2 , and CH_4 was 7.525 W·m⁻², 0.022 mg·(m²·s)⁻¹, and 0.054 μ g·(m²·s)⁻¹, respectively. During the test period, 84%, 80%, and 94% of half-hourly flux data for H_2O , CO_2 , and CH_4 were higher than the zero-gradient measurement precision. ②Based on the measurement, the small pond was the source of CO_2 and CH_4 for the atmosphere in summer, the mean emission flux of CO_2 and CH_4 was 0.038 mg·(m²·s)⁻¹ and 0.889 μ g·(m²·s)⁻¹, respectively. The CH_4 emission fluxes from the small pond were more higher than the median value of emission for global lakes. The results indicated that greenhouse gas emission from small pond was an important part for estimating inland water greenhouse gas emissions, especially for CH_4 emission. These results can provide scientific reference for making emission inventory of regional greenhouse gas.

Key words: small pond; greenhouse gas fluxes; water-air interface; flux-gradient method; eddy covariance method; spectrum analyzer

小型池塘作为一类重要的内陆人工水体,其总面积只占全球水体分布总面积的 8.6%^[1],但相比大型和中型水体,由于小型池塘具有较高的周长面积比和较浅的水深,能够积累更多的外来陆地有机碳作为有机质供池塘底泥微生物进行呼吸作用,因此有利于底泥 CO₂ 和 CH₄ 的产生^[2-6],同时小型池塘较浅的水深导致水体和大气之间能够快速混合交

换,意味着 CH₄ 有更快的排放速度可以减小其在水体中被氧化的几率,有利于 CH₄ 的排放^[7,8]. 基于

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以上原因,小型池塘逐渐成为温室气体排放的研究 热点^[9].并且,根据 Holgerson等^[1]对现有水体温室 气体通量研究统计的结果,小型池塘的 CO₂ 和 CH₄ 排放比例分别占内陆水体总 CO₂ 和 CH₄ 排放的 15.1%和 40.6%.但在过去由于小型池塘面积较小,研究者在估算内陆水体温室气体排放量时通常 将小型池塘忽略掉^[10],而只关注大型或中型水体, 从而导致全球水体温室气体排放估算存在很大的不 确定性,可能会产生低估的现象.因此,研究小型池 塘温室气体交换通量对准确估算全球温室气体交换 通量具有重要贡献.

测定水-气界面温室气体通量的方法主要有箱 式法、水平衡法、微气象学方法和遥感反演法 等[11]. 在野外观测中最常用的方法为前3种. 箱式 法和水平衡法,其装置简单、易于操作,常被使用. 但是,箱式法代表区域小,无法进行高频的测 量[12,13]. 而利用水平衡法进行观测时,观测的甲烷 会产生偏低的现象,因为该方法无法观测到甲烷冒 泡的现象,但在水体中冒泡是甲烷的主要排放方式 之一[6]. 相比这两种方法, 涡度相关方法 (eddy covariance, EC)和通量-梯度方法(flux gradient, FG)等微气象观测方法由于其测量的连续性和对测 量环境的非干扰性已经得到广泛的关注并开始进行 使用[14]. 当前,野外使用的 EC 方法常采用开路式 红外气体分析仪对气体浓度进行测量,但该仪器测 量精度容易受到大气水汽密度和气温波动的影响 (主要影响测量光谱),并且该仪器本身存在的自加 热效应会影响或掩盖地-气交换中较小通量的信 号[15,16]. FG 方法是利用大气气体浓度梯度和气体 湍流扩散系数的乘积来确定地-气气体交换通 量[17]. 根据 Xiao 等[14]的研究,使用高精度闭路式 气体分析仪测量水-气界面温室气体交换通量的 FG 方法最主要的优点是其计算结果不需要进行密度校 正,并且有足够的精度能够观测到甲烷的小梯度和 通量信号. 但在实际应用中 FG 方法也有一定的局 限性,FG 方法中涉及到的重要参数:气体湍流扩散 系数 K,其会受到大气层结条件、气流垂直切变等 湍流外因参数的影响,特别是在大气稳定($\zeta > 0.5$) 和强不稳定($\zeta < -1$)时不容易确定^[18].

长江三角洲地区水域辽阔,水系发达,是良好的水产养殖区域,其中淡水养殖面积为 1.38 × 10¹⁰ m²,占全国淡水养殖面积的 22.7%^[19],这类池塘水-气界面的温室气体交换通量对于大气中温室气体浓度的影响不容忽视,但对于此区域的小型池塘温室

气体交换通量研究还尚不明确. 因此,本研究利用基于离轴积分输出腔光谱技术(off-axis integrated cavity output spectroscopy, OA-ICOS)的分析仪构成的通量-梯度系统于2015年7月15日(日序196 d)至24日(日序205 d)对南京浦浩生态园内的一处小型池塘的水-气界面CO₂、CH₄以及H₂O交换通量进行原位连续观测,以明确:①通量-梯度系统在观测小型水体温室气体通量的性能;②定量估算夏季小型池塘水-气界面温室气体交换通量. 本研究结果可为准确观测及估算内陆水域温室气体交换通量研究提供方法基础及基本数据,同时也为制定渔业温室效应减排政策提供参考.

1 材料与方法

1.1 研究区域

本实验的研究地点设在南京浦浩生态园内的一处'L'型小型鱼类养殖池塘(32.24°N,118.69°E,如图1),占地面积为3 720 m^2 ,平均水深为 1.5 m; 在观测期间,其水体的 pH 和水温平均值分别为 7.9 和 27.4℃. 鱼塘内每天 15:00~16:00 要施加 1 次饵料, 1 次施加量约为 10~20 kg,施加饵料的成分主要有:蛋白质≥32.0%,粗纤维≤9.0%,粗脂肪≥3.5%,粗灰分≤18.0%,总磷≥1.0%,赖氨酸≥1.4%.



图中红色方框包围区域为研究池塘, 红色星星代表通量-梯度系统所在位置

图1 研究区域示意

Fig. 1 Location of the study area

1.2 通量-梯度观测

FG 计算方法的基本假设是在近地层中物质的 传输与其物理属性的梯度成正比,其比例系数即为 湍流扩散系数 $K^{[20]}$,通量-梯度计算方法如公式(1) 所示:

$$F = c\rho_{a}K \frac{r_{1} - r_{2}}{z_{1} - z_{2}} \tag{1}$$

式中,F代表的是气体通量值 $[CO_2: mg \cdot (m^2 \cdot s)^{-1},$ CH₄: $\mu g \cdot (m^2 \cdot s)^{-1}$, H₂O: $g \cdot (m^2 \cdot s)^{-1}$]; $r_1 \neq r_2$ 分别代表在 z_1 和 z_2 高度所测得0.5h气体混合比 [CO_2 : $\mu mol \cdot mol^{-1}$, CH_4 : $nmol \cdot mol^{-1}$, H_2O : μmol·mol⁻¹]. 测量仪器为便携式温室气体分析仪 (型号:915-0011-CUSTOM.美国:Los Gatos Research 公司),其测量原理为离轴积分输出腔光谱技术,该 仪器能够同时测量 CO,、CH4 和 H,O 浓度值,测量 频率为1 Hz,根据用户手册提供,分析仪测量3 种气 体(CO₂、CH₄和 H₂O)的 100 s 测量精度分别为 0.100 μmol·mol⁻¹、0.600 nmol·mol⁻¹ 和 0.060 mmol·mol⁻¹. 本研究中将原始 1 Hz 数据按照上下 进气口分类之后分别计算 30 min 算术平均值; ρ 。 代表空气密度 $(kg \cdot m^{-3})$; c是不同气体的单位转换 常数(CO2:44/29,CH4:16/29,H2O:18/29);湍流 扩散系数 $K(m^2 \cdot s^{-1})$,根据空气动力学原理结合莫 宁-奥布霍夫相似理论进行确定[14],如公式(2) 所示:

$$K = k\mu_* \times z_{\sigma}/\varphi_{\rm h} \tag{2}$$

式中,k 代表 Von-Karma 常数(\approx 0.4); μ_* 代表摩擦风速($\mathbf{m} \cdot \mathbf{s}^{-1}$); $z_{\mathbf{g}}$ 为两个测量高度的几何平均高度 [$z_{\mathbf{g}} = (z_1 z_2)^{1/2}$, \mathbf{m}]; $\varphi_{\mathbf{h}}$ 为关于稳定度参数的普适函数,对于普适函数的确定则使用奥布霍夫稳定方程进行确定,如公式(3)所示;

$$φ_h = 1 + 5ζ \quad (ζ > 0, 稳定条件)$$

$$arphi_{h} = (1 - 16\zeta)^{1/2}$$

($\zeta < 0$,中性或不稳定条件) (3)

式中, ζ 为稳定度参数,利用 $z_{\rm g}/L$ 进行确定,其中 L 为莫宁-奥布霍夫长度 (m),对于 L 值则使用公式 (4)进行确定:

$$L = -\mu_*^3 / [k(g/\theta_v) \overline{\omega'\theta'}]$$
 (4)

式中,g 是重力加速度(\approx 9.8 m·s⁻²), θ_v 是虚位温 (K), $\overline{\omega'\theta'}$ 是动量显热通量(m·K·s⁻¹),对于 μ_* 和 $\overline{\omega'\theta'}$ 可以从涡度相关观测数据计算获得. 对于湍流 扩散系数 K 值,本研究通过将 FG 方法得到的结果 与修正的波文比方法(modified bowen-ratio, MBR 方 法)^[21]计算得到的结果进行比较,验证计算得到 K 值的准确度.

根据 FG 计算原理设计的通量-梯度系统如图 2 所示,放置在距离池塘边1.5 m处:两个进气口位于 小型池塘内,距离水面的高度设置分别为 0.35 m 和 1.05 m,利用外置泵(流速:1.5 L·min⁻¹)对上下进 气口两条管路同时进行抽气并进行气体分析. 气体 在进入分析仪之前,首先通过7 μm 的空气过滤器 (型号:SS-4FW-7, 美国:Swagelok 公司)进行过滤, 之后通过 4 L 的混合瓶使其充分混合(可以保证在 测量过程中不受空气湍流波动的影响),最后利用 电磁阀(型号:T3NCSS-078, 美国:IQ Valves 公司) 对上下进气口的气体进行梯度切换,切换时间为60 s. 并且,为了降低切换对测量的影响,尽量缩短电 磁阀和分析仪之间的距离(实际距离为: 0.1 m). 同时为了防止在夏季夜晚野外观测时通量-梯度系 统管路出现凝露现象,致使仪器抽取水分损坏仪器, 因此,在整个便携式通量-梯度系统内部加了一圈恒 温加热系统,在实验期间设定其温度为30℃.在实 验观测期间,仪器大约需要 25 s 切换后能够达到稳 定状态. 图 3 是在实验观测期间节选的 5 min 气体

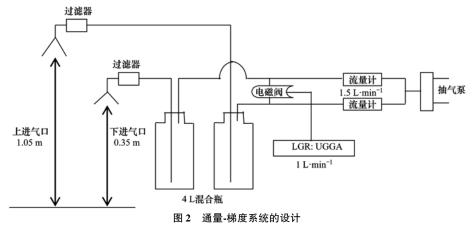
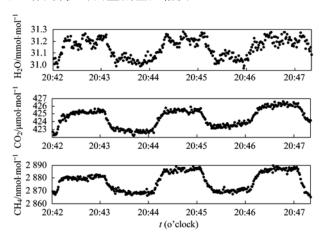


Fig. 2 Schematic design diagram of flux-gradient system

原始浓度变化时间序列,在这 5 min 的测量过程中, 3 种气体 $(H_2O \setminus CO_2 \ n\ CH_4)$ 的浓度梯度差分别为 0.156 mmol·mol $^{-1}$ 、 2.450 μ mol·mol $^{-1}$ 和 15 nmol·mol $^{-1}$,可以证明该通量-梯度系统能够观测到 大气中气体的梯度变化.为了保证通量-梯度系统 具有足够的精度测量水-气界面温室气体交换通量,本研究通过零梯度测试定量验证通量-梯度系统及 配套分析仪的测量偏差及精度.



实验观测期间:2015-07-20(日序: 201 d)20:42~20:47 图3 H₂O、CO₂和 CH₄混合比的5 min 时间序列

Fig. 3 The 5 min time series of H₂O, CO₂, and CH₄ mixing ratios

本实验观测期间的风向玫瑰图如图 4(a) 所示.由于小型池塘附近下垫面类型较多,为保证信号来源全部来自小型池塘内部,因此对数据信号作风向筛选,所选择的风向范围为 92°~106°和 161°~182°,在这两个风向范围内可以保证信号来源不受其他下垫面类型的信号以及仪器支架的干扰,实际观测中 161°~182°风向范围内的数据量较少,因此忽略不计.根据 FSAM 模型[22] 计算得到,在 92°~

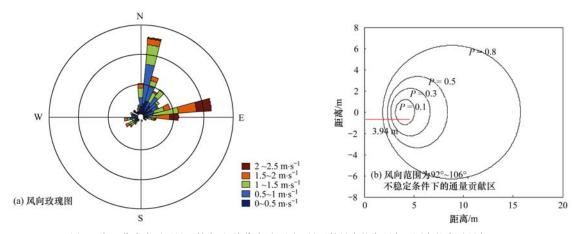
106°风向范围内,大部分数据处于大气层结不稳定条件下,其通量贡献区中对观测通量贡献最大的点距离观测点的水平距离为3.94 m,当其通量贡献率(P)为80%时,通量-梯度方法测定的代表面积约为118 m²[图4(b)],同时结合鱼塘的边界范围,可以保证在92°~106°风向范围内的所有数据信号全部来自小型池塘内部.

1.3 涡度相关观测

本研究中涡度相关观测系统距离通量-梯度系统水平距离为2 m,架设高度距离水面1.5 m,观测仪器主要包括两部分:三维超声风速仪(测量三维风速/超声虚温,型号: CSAT3A,美国: Campbell Scientific 公司)和开路式红外气体分析仪(测量大气H₂O和CO₂密度,型号: EC150,美国: Campbell Scientific 公司),采样频率均为10 Hz,由数据采集器(型号: CR3000,美国: Campbell Scientific 公司)在线计算30 min 平均的动量、感热、潜热和CO₂通量等数据.对EC测量的通量数据后处理过程包括:①根据降水记录值进行剔除;②对数据进行两次坐标旋转^[23];③进行超声虚温订正和密度响应校正(WPL校正)^[16,23].

1.4 修正的波文比方法(modified bowen-ratio, MBR 方法)

MBR 方法主要用来估计痕量气体的交换速率^[21],其基本假设认为所有的气体传输系数(k)值相同,计算公式如公式(5)所示. 假设有两种不同的气体(1号和2号),其气体浓度分别为 c_1 和 c_2 ,其中 F_{c_1} 为已知气体(1号)通量值,并且已知 Δc_1 和 Δc_2 ,分别为1号和2号气体的浓度梯度差,根据MBR 方法的假设,由于所有气体的传输系数k值相



图(b)中P代表水平通量贡献率,红线代表对观测通量贡献最大的点距离观测点的水平距离(m)

图 4 实验观测期间风向玫瑰图及通量贡献区

Fig. 4 Wind rose and flux footprint during experimental observation period

同,因此根据公式(5)即可求得 2 号气体通量 F_{c_2} (假设两种气体两个观测高度差相等,即 $\Delta z_1 = \Delta z_2$, 其中 Δz 已经包括在 k 值的计算中).

$$F_{c_2} = F_{c_1} \frac{\Delta c_2}{\Delta c_1} = k \Delta c_2 \tag{5}$$

在本研究中,由于 EC 观测得到的潜热通量 (latent flux, LE)和 FG 方法观测得到的潜热通量具有较好的一致性(图 5). 因此,利用 EC 观测得到的水汽通量值和 FG 观测到的 H_2O 浓度差结合公式 (5)计算气体交换系数 k,再结合 FG 观测得到的 CO_2 和 CH_4 浓度梯度差,利用公式(5)计算 CO_2 通量和 CH_4 通量,将 MBR 方法计算结果和 FG 计算结果进行对比,验证 FG 方法中对于湍流扩散系数 K值计算的准确度.

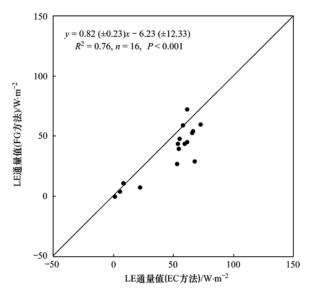


图 5 比较涡度相关和通量-梯度方法计算得到的潜热通量

Fig. 5 Comparison of latent flux(LE) calculated with the EC method and the FG method

1.5 辅助观测

其他辅助观测包括风速风向传感器(型号: 05103,美国:R M Young 公司),架设高度距离水面 3.5 m,测量频率为 1 Hz,为了配合通量数据计算,将风速和风向数据计算为 30 min 矢量平均.

2 结果与讨论

2.1 FG 方法稳定性测试

2.1.1 零梯度测试结果

零梯度测试方法是将通量-梯度系统的两个进气口放置在同一高度上进行测量.本套通量-梯度系统共进行了两次零梯度测试,分别是在实验室内和野外进行.第一次测试时间从日序128 d 的21:30到日序129 d 的19:00,这段期间的数据主要用来分析通量-梯度系统测量0.5 h 气体混合比差(混合比差等于下进气口气体浓度减去上进气口气体浓度)的偏差.第二次测试时间从日序195 d 的16:00到日序196 d 的17:00,这段期间的数据主要用来分析通量-梯度系统测量气体通量的偏差.

零梯度测试期间 3 种气体 $(H_2O_{\circ}CO_2_{\circ}CH_4)$ 0. 5 h 的混合比差的平均值和标准差及频数分布图分别如表 1 和图 6 所示 ,0.5 h H_2O 混合比差的标准差为 0. 006 $\,\mathrm{mmol\cdot mol^{-1}}$,约小于零梯度测试期间大气中 $\,\mathrm{H_2O}$ 浓度 $(19.776\,\,\mathrm{mmol\cdot mol^{-1}})$ 3 个量级;同样地 $,\mathrm{CO_2}$ 和 $\,\mathrm{CH_4}$ 的 0. 5 h 混合比差的标准差分别为 0. 110 $\,\mathrm{\mu mol\cdot mol^{-1}}$ 和 0. 104 $\,\mathrm{nmol\cdot mol^{-1}}$,小于零梯度测试期间大气浓度值($\,\mathrm{CO_2}$:461. 830 $\,\mathrm{\mu mol\cdot mol^{-1}}$,CH₄:2 072 $\,\mathrm{nmol\cdot mol^{-1}}$)的 3 个量级。同时根据图 6 中 3 种气体 0. 5 h 混合比差的频数分布图可以看出 $,\mathrm{H_2O}_{\circ}CO_2_{\circ}CH_4$ 混合比差的变化区间分别为 -0.010 $\sim 0.012\,\,\mathrm{mmol\cdot mol^{-1}}$ 、-0.400 \sim

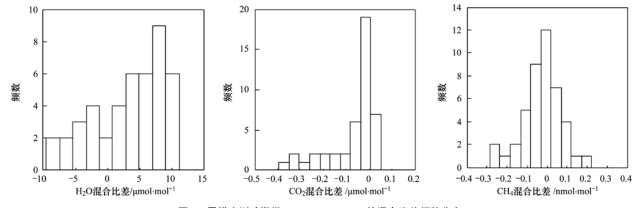


图 6 零梯度测试期间 H_2O 、 CO_2 、 CH_4 的混合比差频数分布

Fig. 6 Frequency distribution of the H2O, CO2, and CH4 mixing ratio differences during the zero-gradient test

0. 100 μmol·mol⁻¹、 - 0. 300 ~ 0. 200 nmol·mol⁻¹. 该结果表明通量-梯度系统测量气体浓度梯度的偏差较小,并且偏差范围分布较为集中.

表 1 零梯度测试期间 0.5 h 的 H_2O 、 CO_2 、 CH_4 的混合比差的平均值和标准差

 $\label{eq:table 1} \begin{array}{ll} \text{Table 1} & \text{Mean value and standard deviation of half-hour H_2O, CO_2,} \\ \text{and CH_4 mixing ratio differences during the zero-gradient test} \end{array}$

项目		混合比差	
- 一 一	$H_2 O/mmol \cdot mol^{-1}$	$CO_2/\mu mol \cdot mol^{-1}$	$\mathrm{CH_4/nmol \cdot mol^{-1}}$
平均值	0.003	-0.070	0. 032
标准差	0.006	0. 110	0. 104

当上下进气口在同一高度进行零梯度测试时, 潜热通量(LE)、 CO_2 通量(F_c)以及 CH_4 通量(F_m) 的理想值应为 0. 本研究零梯度测试的 LE、 F_c 、 F_m 的平均值及标准差和频数分布图分别如表 2 和图 7 所示,零梯度测试期间 LE、 F_e 、 F_m 的平均值(\pm 标准差)分别为 -7.443 (± 7.525) W·m $^{-2}$ 、 -0.004 (± 0.022) mg·(m²·s) $^{-1}$ 和 -0.077 (± 0.054) μ g·(m²·s) $^{-1}$,其量级都较小。同时由图 7 频数分布可知,对于 LE 和 F_e ,其中 80% 的数据所在的范围是 $-11.347 \sim 2.712$ W·m $^{-2}$ 和 $-0.030 \sim 0.030$ mg·(m²·s) $^{-1}$,90% 的 F_m 数据落在 $-0.150 \sim -0.040$ μ g·(m²·s) $^{-1}$ 范围。在零梯度测试期间,湍流扩散系数 K 的平均值和标准差分别为 0.045 m²·s $^{-1}$ 和 0.014 m²·s $^{-1}$,K值的变化范围为 $0.022 \sim 0.075$ m²·s $^{-1}$. 该结果表明通量-梯度系统测量气体通量值具有较低的测量偏差,并且测量偏差分布范围较为集中.

表 2 零梯度测试期间 0.5 h 的 H_2O 、 CO_2 、 CH_4 的通量和湍流扩散系数 K 的平均值和标准差

Table 2 Mean value and standard deviation of half-hour H2O, CO2, and CH4 flux and eddy diffusivity during the zero-gradient test

		2 , 2, 4	, , ,	, 8
项目		通量值		扩散系数
坝目	LE/W·m ⁻²	$F_{\rm e}/{\rm mg}\cdot ({\rm m}^2\cdot {\rm s})^{-1}$	$F_{\rm m}/\mu g \cdot ({\rm m}^2 \cdot {\rm s})^{-1}$	K/m ² ⋅s ⁻¹
平均值	-7.443	- 0. 004	-0.077	0. 045
标准差	7. 525	0. 022	0. 054	0. 014

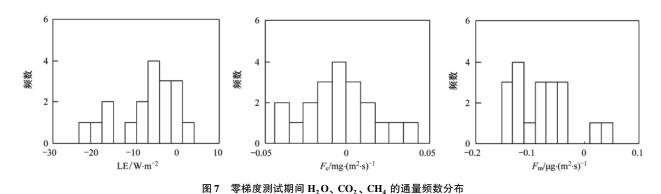


Fig. 7 Frequency distribution of the H₂O, CO₂, and CH₄ fluxes during the zero-gradient test

零梯度测试期间所测得的气体混合比差及通量值的标准差可以作为此套通量-梯度系统及分析仪的测量精度值^[14]. 与其他公开发表文献的零梯度测试结果进行比较,比较结果如表 3 和表 4 所示:①本套通量-梯度系统观测到的 H₂O 和 CO₂ 混合比差较太湖^[14]、Lake Gårdsjön 研究结果^[21]偏高一些,

CH₄ 偏差则较小,总体上处于合理范围之内;②与 文献调研得到的 CH₄ 通量测试结果比较,本研究的 零梯度测试通量结果处于中上等位置.综合以上结 果可以证明本套通量-梯度系统的零梯度测试结果 具有较低的测量偏差,可以保证本套通量-梯度系统 具有足够的精度测量气体交换通量.

表 3 本研究与不同文献中零梯度测试得到气体混合比差的结果1)

Table 3 Gas mixing ratio difference during zero-gradient test in this study and in other literature researches

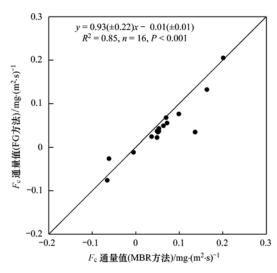
测量地点	测量方法	_	气体混合比差			
侧里地点	例里刀伍	$H_2O/\mu mol \cdot mol^{-1}$	$CO_2/\mu mol \cdot mol^{-1}$	$\mathrm{CH_4/nmol \cdot mol^{-1}}$	文献	
太湖	通量-梯度方法	-0.740 (±20)	-0.033(±0.041)	0.200(±0.360)	[14]	
Lake Gårdsjön	通量-梯度方法	-1.100 (±3.200)	$0.033 (\pm 0.026)$	_	[21]	
水稻田	通量-梯度方法	_	_	0. 200	[18]	
小型池塘(本研究)	通量-梯度方法	3.320 (±5.550)	$-0.070 (\pm 0.110)$	$0.032 (\pm 0.104)$	本研究	

¹⁾括号中的数字代表相应的标准差;"一"表示文献中没有相关数据,下同

表 4 本研究与不同文献中零梯度测试得到气体通量的结果

Table 4	Gas flux durii	g zero-gradient tes	st in this study	v and in othe	r literature researches

测量地点	测量方法		气体通量值			
侧里地点	侧里刀法	LE/W·m ⁻²	$F_{\rm c}/{\rm mg} \cdot ({\rm m}^2 \cdot {\rm s})^{-1}$	$F_{\rm m}/\mu g \cdot (m^2 \cdot s)^{-1}$	文献	
太湖	通量-梯度方法	-0.050 (±4.800)	$-0.008(\pm 0.010)$	0.016(±0.029)	[14]	
泥炭地	闭路式箱式法 波文比能量平衡法	_ _	_ _	0. 026 0. 600 ~ 7. 080	[24]	
乳牛场	涡度相关方法	_	_	$0.670(\pm 0.530)$	[25]	
池塘	自动箱式法	_	_	0. 053	[12]	
小型池塘(本研究)	通量-梯度方法	$-7.443(\pm 7.525)$	$-0.004(\pm 0.022)$	$-0.077(\pm 0.054)$	本研究	



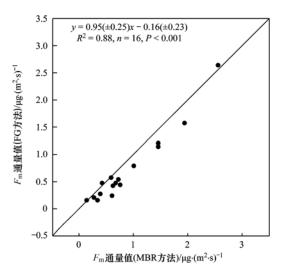


图 8 比较由 MBR 方法和 FG 方法计算的 F_c 和 F_m 通量值

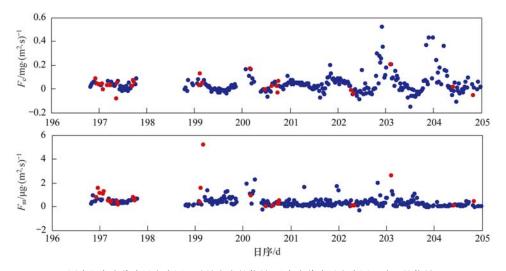
Fig. 8 Comparison of CO₂ flux (F_c) and CH₄ flux (F_m) measured by the FG method with that calculated by the MBR method

2.1.2 FG 和 MBR 方法计算结果比较

FG 方法和 MBR 方法所计算得到的 CO, 和 CH4 通量比较结果如图 8 所示. 对于 F_{c} , 两种计算方法 得到结果的平均误差(mean error, ME, FG-MBR)、 均方根误差(root mean squares error, RMSE)以及一 致性指数 (index of agreement, IOA) [26] 分别为 $-0.010 \text{ mg} \cdot (\text{m}^2 \cdot \text{s})^{-1}, 0.028 \text{ mg} \cdot (\text{m}^2 \cdot \text{s})^{-1}$ π 0.948. 对于 F_m , 两者的 ME、RMSE 以及 IOA 分别 为 - 0.147 $\mu g \cdot (m^2 \cdot s)^{-1}$ 、0.180 $\mu g \cdot (m^2 \cdot s)^{-1}$ 和 0.968. 以上的比较分析结果表明, MBR 方法和 FG 方法计算的 CO, 和 CH。通量之间具有较小的误差 和较高的一致性,因此可以判断 FG 方法中对于 K值的计算是准确的. 并且,在实验观测期间大气稳 定度 ζ 所处范围 $-0.2 \sim 0.2$, 有利于 K 值的计算. 通过以上对零梯度测试结果以及 FG 方法和 MBR 方法计算结果的比较,可以证明本套通量-梯度系统 具有较高测量精度,并且可以用于水-气界面气体交 换通量的观测.

2.2 小型池塘温室气体排放通量

正常观测期间 CO, 和 CH₄ 通量的时间序列如 图 9 所示,其分别表示了来自陆地与池塘的通量信 号. 为更加清晰了解池塘的温室气体通量排放强度 及变化范围,只挑选来源于池塘信号温室气体通量 数据进行分析. 实验观测期间,池塘水-气界面 CO。 通量有80%的数据高于零梯度测试精度[CO,: 0.022 mg·(m²·s)⁻¹], 其平均排放量为 0.038 (±0.060) mg·(m²·s)⁻¹, 变化范围为 - 0.066 ~ 0.207 mg·(m²·s)⁻¹,在整个测量时间段出现吸收 峰值和排放峰值的时间分别为日序 197 d 的 09:00 和日序 203 d 的 02:00. 观测的 CH4 通量有 94% 的 数据高于零梯度测试精度「CH₄: 0.054 $\mu g \cdot (m^2 \cdot s)^{-1}$],其平均排放量为 0.889(±1.051) $\mu g \cdot (m^2 \cdot s)^{-1}$, 变 化 范 围 为 0.040 ~ 5.239 $\mu g \cdot (m^2 \cdot s)^{-1}$,在整个测量时间段出现最低值和最 高值的时间分别为日序 200 d 的 11:00 和日序 199 d的03:30.



图中红色点代表风向来源于池塘方向的信号,蓝色点代表风向来源于陆地的信号

图 9 CO₂ 和 CH₄ 通量的时间序列

Fig. 9 Time series of CO2 and CH4 flux

表 5 不同时间段的 CO_2 及 CH_4 通量值 $^{1)}$

Table 5 CO2 and CH4 fluxes in different time periods

项目	$00:00 \sim 06:00 \ (n=8)$	$06:30 \sim 12:00 \ (n=6)$	$12:30 \sim 18:00 \ (n=7)$	$18:30 \sim 23:30 \ (n=5)$
$F_{\rm c}/{\rm mg}\cdot ({\rm m}^2\cdot {\rm s})^{-1}$	0.076 (0.068)	-0.006 (0.051)	0.018 (0.038)	0.063 (0.040)
$F_{\rm m}/\mu g \cdot (m^2 \cdot s)^{-1}$	1.662 (1.475)	0. 194 (0. 152)	0.483 (0.278)	1. 215(0. 370)

1)n代表相应时段的数据量;通量后面括号里的数值代表相应时段的标准差

为清晰了解池塘温室气体交换的日变化特征, 对温室气体通量按照不同的时间段进行统计分析. 将一天分为4个时间段,不同时间段对应的气体通 量值如表 5 所示,对于 CO, 通量,池塘白天水-气界 面 CO₂ 通量总体为净排放,其平均值为 0.006 mg·(m²·s)⁻¹,排放量值较小,主要是在 06:30~ 12:00这段期间出现了 CO, 的净吸收现象, 而在夜 晚全部为净排放,其排放量平均值为 0.070 $mg \cdot (m^2 \cdot s)^{-1}$,远高于白天排放值. 决定水体是 CO, 的源还是汇主要取决于水体新陈代谢的结果[4] 当 水体中的水生植物进行光合作用的强度高于水体中 植物及微生物呼吸作用强度时,池塘作为 CO。的 汇,反之呼吸作用占主导因子时,池塘作为 CO,的 源. 白天池塘中的水生植物进行光合作用吸收固定 二氧化碳,当光合作用大于呼吸作用时,可能会产生 部分 CO, 吸收现象,而在夜晚由于没有太阳辐射, 植物以及底泥的微生物只进行呼吸作用,释放 CO。, 因此池塘呈现 CO, 排放源. 总体来说该小型池塘在 夏季表现为 CO, 的排放源. 对于 CH4 通量,在夏季 小型池塘为排放源,并且在夜晚排放的平均值 $[1.439 \, \mu g \cdot (m^2 \cdot s)^{-1}]$ 高于白天排放的平均值 [0.339 μg·(m²·s)⁻¹]. 甲烷主要是底泥中甲烷细 菌在厌氧条件下分解有机质而产生的^[27].本研究中 CH₄ 的排放值夜晚高于白天,一方面由于夜晚池塘植物及微生物进行呼吸作用时会消耗大量氧气,产生厌氧环境,这有利于甲烷的产生;另一方面,由于池塘水深较浅,白天强烈的太阳辐射会导致池塘出现上层水温高于下层水温的稳定热力层结情况,不利用甲烷的扩散,而在夜晚水体辐射冷却出现下层水温高于上层水温的不稳定热力层结,水层容易混合,因此更有利于甲烷的传输^[28].

为了明确该小型池塘夏季温室气体排放量值在不同区域、不同气候条件下小型水体排放量值中所处的水平,同时也为了解在不同地区、不同气候条件及不同季节的条件下,造成小型池塘温室气体排放差别的可能原因,将本研究结果与已有研究结果进行对比,其中杨平等^[29]在 2011 年 10 月 20 ~ 21 日使用箱式法测量闽江口养虾塘(面积:330 m²; 平均水深:0.8 m)和鱼虾混养塘(面积:650 m²; 平均水深:1.0 m)水-气界面温室气体交换通量,观测结果显示在秋季 2 个养殖塘全天整体上表现为 CO₂的汇和 CH₄的源,其中养虾塘 CO₂和 CH₄通量的平均值分别为 - 0.014 mg·(m²·s)⁻¹和 0.280μg·(m²·s)⁻¹,鱼虾混养塘 CO₂和 CH₄通量的平均

值分别为 - 0.029 mg·(m²·s)⁻¹ 和 1.590 μg·(m²·s)⁻¹,与本研究结果小型池塘在夏季为大 气 CO, 的源不同,闽江口的两个养殖塘在秋季都表 现为大气 CO₂ 的汇,产生差异的原因主要是由于两 者水体中水温和初级生产力水平不同有关. 其中本 研究观测在夏季,观测期间水温的变化范围为 26.1 ~30.5℃,平均值为27.4℃,一方面当水温较高时 会加快水中微生物分解作用,另一方面本研究池塘 的有机质浓度主要来源于底泥残余有机饲料、腐败 水草等,池塘内的水生植物较少,因此当在整体光合 强度较弱的条件下,呼吸强度占主导因素,小型池塘 表现为 CO。的排放源. 而闽江口池塘观测研究在秋 季,其池塘的水温变化范围为 19.5~20.6℃,平均 值为20.5℃,其水温相对本研究较低,并且闽江口 研究的两个养殖塘其水体有机质主要来源于水体中 较多的水生浮游植物,其含有较多能够反映光合作 用水平的叶绿素 a^[30],因此整体光合作用强度高于 呼吸作用强度,最终池塘表现为 CO, 的汇.

利用箱式法对瑞典 Linköping 大学附近的一处 小型浅水池塘(面积:1200 m²,平均水深:1.2 m,观 测时间 2010-06-21 ~ 2010-10-10) 温室气体通量观 测研究结果表明[31],其小型池塘生长季节里的 CH4 和 CO₂ 平均排放量分别为 1.480 (± 0.570) $\mu g \cdot (m^2 \cdot s)^{-1}$ 和 0.001 (± 0.004) $m g \cdot (m^2 \cdot s)^{-1}$, 总 体为温室气体的排放源,与本研究结果类似,但是与 本研究的量值存在差异. 本研究的小型池塘的 CH₄ 排放量偏小,主要是由于高纬度水体中存在更多的 有机质,因此产生 CH4 的底物较为丰富,从而会出 现较高的 CH4 排放量. 同时与该研究比,本研究的 CO, 的排放量偏高,产生此现象的原因除了与高纬 度地区气温低于本研究亚热带区域,从而不利于 呼吸作用之外,还与池塘的生产力有关,此研究的 小型池塘含有大量的水生植物(包括芦苇、宽叶香 蒲和眼子菜等),其光和作用强度相比本研究较 高,因此,在高光合作用及较低的呼吸作用下, Linköping 大学附近的小型浅水池塘 CO₂ 排放量偏 小. 根据 Holgerson 等[1]的调研统计结果,其中处 于 0.001~0.01 km² 范围内的水体温室气体(CO2 和 CH₄)排放通量分别为 0.040(±0.010) $mg \cdot (m^2 \cdot s)^{-1}$ 和 0.160 (± 0.040) $μg \cdot (m^2 \cdot s)^{-1}$, 本研究中长江三角洲地区小型池塘的结果与其相 比,CO,排放量相当,本研究的CH。排放量高于调 研统计的 CH₄ 排放量,这主要是由于 Holgerson 等[1]在调研统计过程中对于 CH4 通量,只考虑了 CH₄ 以扩散方式排放的通量,并没有计算以冒泡形式排放的 CH₄ 通量,而相比扩散,在水体中以冒泡形式排放的甲烷所占比例约为 50% ^[6],特别是在浅水湖泊^[31]、热溶喀斯特池塘^[32]和水体边缘^[27]等区域容易产生甲烷冒泡现象.因此,忽略甲烷以冒泡形式排放的通量会产生严重低估现象,而本研究所使用的通量-梯度方法可以观测到 CH₄ 以所有方式排放的通量值,因此 CH₄ 排放量较 Holgerson 等^[1]的调研结果偏高.

进一步了解池塘温室气体排放过程中 CO₂ 和 CH₄ 所占的比例. 本研究结果表明, CO₂ 和 CH₄ 含碳比值为 12. 26, 而百年尺度上甲烷的全球温室潜能是相同质量 CO₂ 的 25 倍^[33],将 CH₄ 转换为 CO₂ 当量之后,其含 C 通量比值(CO₂/CH₄)为 1. 35. 而 Holgerson 等^[1]的统计结果表明处于 0. 001 ~ 0. 01 km² 范围内的水体的 CO₂ 和 CH₄ 排放碳通量的比值为 3. 57, 并且随着水体面积范围的增大,其比值不断增加. 本研究与文献的调研结果都表明小型池塘在温室气体排放过程其 CH₄ 相比 CO₂ 占有更重要的角色. 本研究结果 C 通量比值更低的原因同样是因为,在通量估算过程中,文献统计结果只考虑了扩散,而没有对甲烷冒泡通量进行考虑,对甲烷的排放产生了低估.

3 结论

- (1)零梯度测试结果表明本套通量-梯度系统具有较高的测量精度和较小的测量偏差,并且在正常实验观测期间通量观测数据(H₂O、CO₂和 CH₄)分别有84%、80%和94%的结果高于零梯度测试精度.同时将本研究的零梯度测试结果与其他文献零梯度测试结果对比,本研究的测试结果处于中上等位置,再次表明本套通量-梯度系统有足够的测量精度满足温室气体交换通量的观测.
- (2) FG 方法测得的 CO_2 与 CH_4 通量和 MBR 方法计算结果具有较好的一致性,表明 FG 方法中对于 K 的计算准确.
- (3)基于通量-梯度观测本研究的小型池塘在夏季为 CO_2 和 CH_4 的排放源,观测期间其排放量分别为0.038(±0.060) $mg\cdot(m^2\cdot s)^{-1}$ 和0.889(±1.051) $\mu g\cdot(m^2\cdot s)^{-1}$,夜晚温室气体排放量高于白天排放值,并且小型池塘中 CH_4 排放相比 CO_2 排放占有更重要的角色.
- (4)本研究的结果由于只进行了夏季的观测, 因此无法清晰了解小型池塘温室气体通量的季节动

态变化特征,为了准确定量估算内陆水体中小型池塘的温室气体排放量特别是 CH₄ 排放量,在未来的工作中需要进行长期连续的温室气体交换通量测量,在长期测量过程中,应配套使用稳定性更佳的分析仪,并且注意在平时加强仪器维护工作,以期得到更完善的测量结果,为准确估算区域水体温室气体交换通量提供科学依据.

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《环境科学》多项引证指标名列前茅

2016年10月12日,中国科学技术信息研究所在中国科技论文统计结果发布会上公布了2015年度中国科技论文统计结果. 统计结果显示《环境科学》2015年度总被引频次8844,影响因子1.617,多项引证指标位居环境科学技术及资源科学技术类科技期刊前列.

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